# THE COORDINATING COMMITTEE ON GREAT LAKES BASIC HYDRAULIC AND HYDROLOGIC DATA

# HYDROMETEOROLOGY AND MODELING SUBCOMMITTEE

# HYDROMETEOROLOGICAL DATA COLLECTION DESIGN AND ANALYSIS FOR THE LAKE ONTARIO DRAINAGE BASIN

FINAL REPORT - PHASE I

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#### Prepared for:

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#### Preface

In February 1989, the Hydrometeorology and Modeling Subcommittee of the Coordinating Committee on Great Lakes Basic Hydraulic and Hydrologic Data agreed to undertake an analysis of the existing hydrometeorological data collection network over the Lake Ontario drainage basin.

A coordinated Statement of Work was generated between participants in October 1989. In March 1990, the U.S. National Weather Service, sponsored by the U.S. Army Corps of Engineers, requested proposals to conduct this research. In June 1990, the U.S. National Weather Service awarded a contract to the Hydex Corporation, of Vienna, VA, under Contract 50-WCNW-0-06043 to "Provide Research and Development for Hydrometeorological Data Collection Design and Analysis for the Lake Ontario Drainage

The accepted proposal called for a three-phase, three-year investigation to evaluate the adequacy of the existing rainfall/ snow collection networks maintained around the basin, the relationships of these ground-based observations to airborne snow and soil moisture collection networks, and the use of data collected from these networks in water supply / water level simulation and forecasting models developed for the lake and its drainage basin.

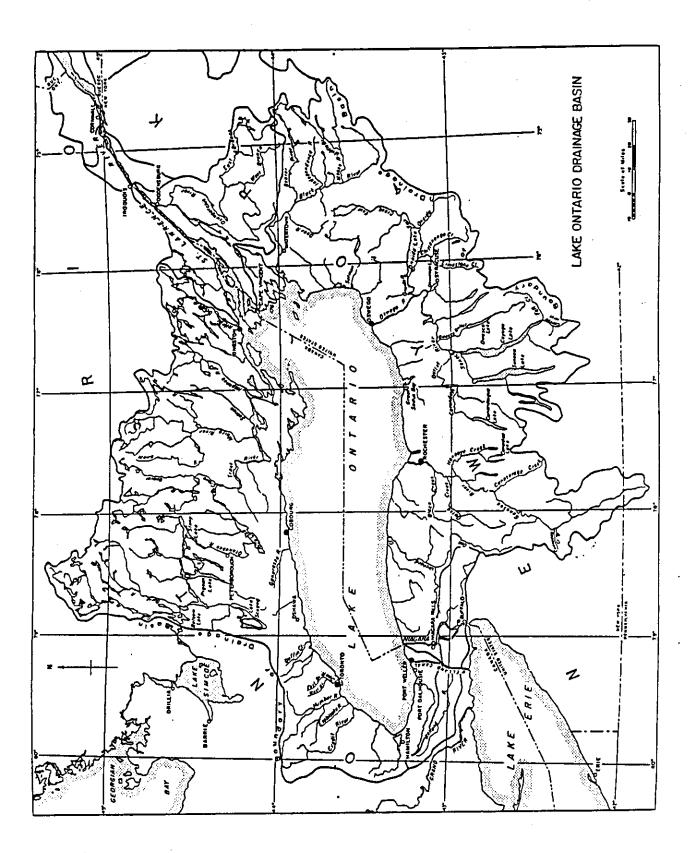
In February 1991, the Hydrometeorology and Modeling Subcommittee agreed to publish the reports of Hydex Corporation, under its authority. This report is the final report for Phase I of the study. Additional reports are expected to be generated for each of Phase II and Phase III, with a composite volume due upon completion of all study activities. Information on the activities to be conducted under Phase II and III can be provided by the Great Lakes Hydraulics and Hydrology Branch, U.S. Army

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#### Table of Contents

$\mathbf{p}_i$	<u>age</u>
Lake Ontario Drainage Basin	V
Lake Ontario Final Report - Phase I	
Development of Data Base	1
Processing of Data	2
Paper for IAGLR Meeting	<u>2</u> .
Attachment A - United States Data Base	5
Accachment A-1 U.S. Stations	9
Attachment A-2 Beaver Fall, Ny Monthly	15
Attachment A-3 U.S. Snow Survey Data	17
Attachment A-4 Snow Survey Stations in U.S	19
Attachment B - Canadian Data Base	23
Attachment B-1 Canada Snow Course Data	27
Attachment B-2 Canadian Snow Courses	29
Attachment C - Adjustment Techniques for Precipitation Records	~ -
Figure C-1 Effect of Wind Speed on Catch of U.S.	3 T
	41
Buffalo, 1989-90	42
Buffalo, Feb-Mar 1989	42
U.S. Precipitation Gages	43
I I The state of the stat	
U.S. Precipitation Gages without Windshields . Figure C-6 Computation of Deficiency in Catch of Snowfall	44
I INTERNATION THE COLUMN OF DISCONTINUING	
U.S. Precipitation Gages with Windshields	45
Figure C-7 Effect of Wind Speed on Catch of Canadian	
Nipher Snow Gage	46
rigure C-8 Computation of Deficiency in Monthly Catch of	
Rain, Canadian Standard Rain Gage	47
Figure C-9 Computation of Deficiency in Monthly Catch of	
Snowfall, Canadian Nipher Gage	48
ttachment D - Consistency and Quality Evaluation of Records .	49
rigure D-1 Double mass Plot of Highmarket, NY Oct-Apr	
Precipitation with Average of Base Stations .	51
eferences	
	53



### Hydrometeorological Data Collection Design and Analysis for the Lake Ontario Drainage Basin

#### FINAL REPORT - PHASE I MAY 24, 1991

This work has been accomplished by the Hydex Corporation, Vienna, Virginia, under contract, 50-WCNW-0-06043, with the National Weather Service (NWS), National Oceanic and Atmospheric Administration (NOAA), Department of Commerce. The work has been sponsored by the U. S. Army Corps of Engineers (COE).

#### DEVELOPMENT OF DATA BASE

The primary effort during Phase I has been the development of the historical hydrometeorological data base and the preparation of the attached reports listing the locations and periods when snow cover measurements have been observed. The data base contains records for stations in those areas in Canada and the United States that drain directly into Lake Ontario. The time period for the study, determined through coordination with the NWS and the COE officials, is the 30-year period, 1961 to 1990 (where available, records are included in the data base starting in January 1955).

Information on records included in the data base for the US and Canadian drainage areas are presented in **Attachment A** (US) and **Attachment B** (Canada). The data base includes some, but not all, of the following records:

Climate Stations

Daily (and Monthly) Precipitation

Temperature (mean daily and/or mean monthly)

Snow on Ground (daily)

Snowfall (daily)

Hourly Precipitation Stations (Monthly totals only)

Synoptic Stations

Daily (and Monthly) Precipitation

Temperature (mean daily and/or mean monthly)

Snow on Ground (daily)

Snowfall (daily)

Wind Movement (mean daily and/or mean monthly)

Snow Surveys

Ground

Remotely sensed (airborne gamma)

As may be seen from the information in Attachments A and B, the data bases for the US and Canada are large and fairly comprehensive.

Most of the hydrometeorological records for the study area were not readily available and not in formats convenient for performing the planned analyses.

However, most records required for the initial and final quality evaluation of the records resides on the Hydex computer system.

Many agencies in Canada and the United States have been very cooperative in furnishing records. In Canada, these include the Canadian Atmospheric Environment Service (AES), Toronto, Ontario, the Ministry of Natural Resources, Toronto, Ontario, and Environment Canada, Parks Service, Peterborough, Ontario. In the United States, the Great Lake Environmental Research Laboratory (GLERL), the US Army Corps of Engineers (COE), the Northeast Climate Center of Cornell University, the NOAA (NWS). Information on the Lake Ontario drainage basins have been furnished on maps by the COE.

## PROCESSING OF DATA

Monthly values of the hydrometeorological records (precipitation, temperature, snow on ground, snowfall and wind movement) are in tabular files with yearly values computed for annual, October-April and May-September periods and 30-year averages for stations that have complete records for the base period. These yearly totals, and 30-year averages for the same seasonal periods, are required to evaluate and Canada have been collected, processed and placed in tables.

A sample set of records has been evaluated for consistency and accuracy during Phase 1.

# Problems with Respect to Data Base

One problem that is difficult to solve is obtaining adequate information on the history of stations sites (precipitation gages and ground snow surveys), such as information on current measurement sites, previous measurement locations, and on changes in equipment or observing techniques. This information is required for evaluation, and where indicated, for adjustment of records.

For the US precipitation stations, a complete set of available station history forms (Report on Substation and Cooperative Station) have been reproduced from NWS records and are on hand at Hydex. During the last few years the NWS has discontinued having the Substation Network Specialists prepare diagrams of the area surrounding a precipitation gage on their Report on Substations. Current instructions are to only provide limited digital information as to distances to obstructions, height of obstructions and angle from the orifice of a precipitation gage to top of the obstructions. Without these diagrams to provide information on all objects and terrain features in the area of a site that relate to exposure of a precipitation gage, the value of greatly reduced. Consideration should be given to alleviating this problem by having precipitation stations in northern areas that receive considerable snowfall along with

the digital information they are presently providing.

Station history information as to dates stations were moved are available for Canadian precipitation stations, but detailed descriptions of most stations are not available. Information on the exposure of Canadian synoptic stations equipped with Nipher gages has been furnished by the AES.

Station history information for US snow survey measurement sites such as moves, description of sites, and description of observing techniques or number of measuring points obtain for each survey is available for only a limited number of stations.

#### Adjustment for Errors in Precipitation Measurement

A review of the literature on techniques for adjusting precipitation for errors due to wind effect and other factors has been accomplished. Adjustment procedures for use in the current project have been developed but have not been finalized. A summary, discussing the adjustment techniques for use in this project, is presented in **Attachment C**. The basic procedures were developed by Hydex in a study for the Environmental Protection Agency (EPA) during which precipitation records for specific locations in northeast US and southeast Canada were adjusted for errors due to wind action at the time precipitation occurred. Most of the Figures in Attachment C were developed during the EPA study using synoptic stations records in the United States and Canada. 1/ Records for the Canadian stations were furnished by AES and considerable advice and information for the development of the procedures were received from Barry Goodison of AES.

#### Quality of Snow Survey and Precipitation Measurements

All snow survey records for the Lake Ontario drainage areas in Canada and the United States have been obtained and are on the Hydex computer. These records have been checked with published records. Snow density values were computed for each snow survey and were reviewed to insure that the values were consistent with those of surrounding stations and for the climate conditions. Information on locations of ground snow surveys have been obtained and tables presenting this information are in Attachments A and B.

The consistency of the snow survey records will be checked using techniques similar to those being used for precipitation records. However, evaluation of the quality of the records for representing areal average snow conditions is difficult to accomplished. The value of the ground snow survey records is determined to a major

11 "Precipitation Data Analysis for Evaluation of Regional Acid Rain Deposition Simulation Models," Final Report, Hydex Corporation to EPA for Modeling Subgroup, Atmospheric Sciences and Analysis Workgroup 2, Under MOI signed August 5, 1980, by United States and Canada. March 1982.

extent by the exposure conditions for the site of the measurement(s). Airborne snow survey records (that are considered to be more representative of areal conditions) will be used during Phase II and Phase III of the project to determine how representative the ground records are for computing areal averages of the water equivalent of the snow cover. Comparison of ground snow survey records with airborne gamma radiation survey records has been postponed until additional records of the airborne surveys are available.

Evaluation of the quality of the precipitation measurements (rain and snowfall) has been initiated. Double mass plots of the winter measurement of precipitation have been prepared. A brief discussion on this work is presented in **Attachment D**.

# PAPER FOR IAGLE MEETING

An invitation was received to present an invited paper at the International Association for Great Lake Research, IAGLR, annual conference to be held in Buffalo, New York, June 2-6, 1991. The paper "Evaluation of Ground and Airborne Data for Snowmelt Forecasting for Lake Ontario Basin," has been accepted and will be presented in the "Forecast and Prediction Systems" session on June 3, 1991.

# Hydrometeorological Data Collection Design and Analysis for the Lake Ontario Drainage Basin

FINAL REPORT - PHASE I MAY 24, 1991

ATTACHMENT A

#### **UNITED STATES DATA BASE**

#### CLIMATE RECORDS

## **Daily Precipitation Records**

Daily precipitation values from 1955-1990 for the 93 stations listed in **Attachment A-1** are on hand at Hydex. The records were obtained primarily from the NOAA Library in Rockville, Maryland and the Washington NWS offices.

Monthly values were computed from the daily values and put in tabular form with annual, Oct-Apr and May-Sep totals and with 30-yr monthly and seasonal average values. Missing monthly values for the period 1961 to 1990 for longer record stations were estimated from nearby stations. In the publication of the daily precipitation records in the Monthly Climatological Bulletins, the US practice is to have a "M" appended to the monthly total if 1-9 daily values are missing. If 10 or more days are missing no monthly total is published. Missing data for partial periods in 1989 and 1990 were estimated based on average relationships with nearby stations. Some monthly totals, prior to 1989, that were computed from the records of daily precipitation values available on CD ROMS have periods of missing data. These records need to be checked and values for these periods estimated from nearby stations. A sample of a monthly data form, containing the average values and dates of months with missing records that were estimated from nearby stations, is shown in **Attachment A-2**.

The standard precipitation gage at climate stations of the NWS has a collector of 8-inch (20.3 cm) diameter that is mounted with its orifice about three feet above the ground. This is the gage used to collect measurements of the daily amount of precipitation (rain and snowfall) at about 90 cooperative weather stations (daily climate stations) in and adjacent to the Lake Ontario drainage area. This is a manual gage with an inside tube (the measuring tube) that is 1/10 the area of the larger collector and a funnel on top of the overflow can of the gage. Rainfall is measured by inserting a measurement stick in the inside tube and measuring the amount of precipitation from the scale on the measurement stick. When snowfall is anticipated, the inside tube and the funnel are removed and the snowfall allowed to fall directly into the large overflow can. The amount of snowfall is measured by allowing the snow in the overflow can to melt or by pouring into the overflow can a measured amount of

warm water and pouring the liquid into the measuring tube to measure the snowfall as you do for rain (correcting for the warm water added if this was done).

## **Hourly Precipitation**

Records of daily amounts of precipitation at hourly precipitation stations (recording precipitation stations) required for use in initial evaluation analyses have the NOAA Library or NWS offices.

Several different recording gages are used at about 30 recording stations (most of which are also daily climate stations) in and near Lake Ontario for which hourly amounts of precipitation are published. The three most common recording gages are the tipping bucket, the weighing-type gage (often referred to as the universal gage), and a punched tape recording gage (the Fischer-Porter). All recording gages are mounted with the gage orifice about four to five feet above ground, except when occasionally mounted on roofs of buildings. Windshields (alter type) in the Lake Ontario basin are installed almost exclusively on gages at synoptic weather stations.

## Temperature Records

Temperature records are available for a large number of stations listed in Attachment A-1 (most of these stations also report daily precipitation, snowfall, snow on the ground, and a few report water equivalent of snow on the ground). Sample records have been obtained for those stations required for demonstration purposes. Records for all other stations are available at the NOAA Library or NWS offices.

#### Snowfall

Records of daily snowfall for some of the climate stations have been obtained. Records for remainder of basin stations are available from the NOAA Library or NWS offices.

## Snow on Ground

A sample set of records of daily snow on ground data have been obtained. Records for rest of stations that record snow on ground are available from the NOAA Library or NWS offices.

## Station History Information

Copies of forms containing station histories information for stations listed in Attachment A have been obtained and on file at Hydex. This constituted a major undertaking. However, station history information is now available for all precipitation stations (daily, hourly and synoptic) in and immediately adjacent to the US drainage

area. These station history files were obtained from micro-fiche at the NOAA Library and by copying original forms at NWS for the last few years. This was accomplished at this time since experience has shown that the forms for the last few years are often unavailable for long periods of time when the forms for the latest years are sent to be placed on micro-fiche.

#### Wind

Daily wind movement records for Syracuse, New York, have been obtained from NWS files and are on the Hydex's computer. Tim Hunter, Great Lakes Environmental Research Laboratory (GLERL), has furnished daily wind records for the last few years for most synoptic stations in Canada and in the US. He has also furnished daily wind records for the Watertown Airport station for the period 1949-64 and for the last four months of 1988. Daily wind records for the Watertown Airport station were obtained for the period 1989-1990 from the Detroit Office of the COE.

#### SNOW SURVEYS

#### Snow Surveys (Ground)

Keith Eggleston, Northeast Climate Center, Cornell University has furnished a tabulation of historical snow course records (from 1957-1990) for the State of New York. The first and last pages of the table, US Snow Surveys Data, Lake Ontario Basin, listing all records for stations in study area is shown in **Attachment A-3**. A list of snow survey locations is presented in the table, Snow Survey Stations in US, Lake Ontario Basin, shown in **Attachment A-4**.

## Snow Surveys (Airborne Gamma)

Airborne gamma radiation surveys of the water equivalent of the snow were obtained from Thomas Carroll (NWS) for 42 flight lines flown on March 1-3, 1990, using the NWS Airborne Gamma Radiation System. Earlier surveys were made over the Lake Ontario basin by the NWS during IFYGL in 1973 and 1974 but are not usable since the airborne gamma radiation system has changed.

Information as to location of each flight line, digitized longitude and latitude, for the beginning and end points of the 42 established flight lines was received. A map showing the flight lines has also been furnished by Tom Carroll (NWS).

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STATE-STATION	30 YF	FYI	UMRER	LAT	LONG	FLEV	252100 25			NT A-1 WIND
NEW YORK			IOMOEN	LAI	LONG	FT	RECORD	DATA		ENSOR
		2/				MSL	/3		14	
ALBION 3 ENE			30-0055	43.25	78.13	510	/3 5/1948 - 12/1988	PP24	74	
ALFRED	20		20.0005	40.05	77 00	1740	5/1948 - 12/1988 1/1926 - 12/1988 1/1926 - 12/1988	SNOG	70	
ACI IIED	30		20-0085	42.23	77.80	1740	1/1926 - 12/1988	SNOF	99	
ANGELICA	30		30-0183	42.30	78.03	1420	1/1926 - 12/1988	PP24	99	
							1/1926 - 12/1988	SNOF	93	
100105							1/1926 - 12/1988	SNOG	88	
ARCADE			30-0220	42.53	78.42	1490	5/1948 - 12/1988	PP24	93	
							5/1948 - 12/1988 5/1948 - 12/1988	SNOC	93	
AURORA RESEARCH FARM	30		30-0331	42.73	76.65	830	11/1958 - 12/1988	PP01	98	
							11/1956 - 12/1988			
							11/1956 - 12/1988	SNOF	98	
							11/1956 - 12/1988	SNOG	98	
AUBURN 2 NE			30-0321	42.92	76.53	770	1/1926 - 11/1987	PP24	83	
							1/1926 - 11/1987	SNOF	83	
							1/1926 - 11/1987			
AVON			30-0343	42 95	77 73	560	2/1989 - 12/1990 5/1948 - 12/1988			
			50 0543	72.33	11.13	300	5/1948 - 12/1988			
							5/1948 - 12/1988	SNOG	6.3	
BALDWINSVILLE	30		30-0379	43.15	76.33	380	5/1948 - 12/1988	PP24	97	
							5/1948 - 12/1988	SNOF	89	
BARNES CORNERS							5/1948 - 11/1988	SNOG	6.5	
BARNES COHNERS			30-0424	43.82	75.80	1520	11/1979 - 12/1988	PP24	93	
							11/1979 - 12/1988 11/1979 - 12/1988			
BATAYIA	30		30-0443	43.00	78.18	900	12/1984 - 12/1988	PP01	92	
				10.00	, _ , , ,	•••	5/1948 - 12/1988			
							5/1948 - 12/1988			
D. T.							5/1948 - 12/1988	SNOG	94	
BATH			30-0448	42.33	77.33	1110	8/1953 - 12/1988			
							8/1953 - 12/1988 8/1953 - 12/1988	SNOF	95	
BEAVER FALLS	30		30-0500	43 88	75 43	740	5/1948 - 12/1988	DD24	95 98	
			*******	40.00	70.40	, ,,	5/1948 - 11/1988	SNOF	92	
							5/1948 - 12/1988	SNOG	91	
BENNETTS BRIDGE	30		30-0608	43.53	75.95	660	5/1948 - 12/1988	PP24	98	
							5/1948 - 12/1988	SNOF	98	
BIG MOOSE 3 SE	• •		30-0668	40.00	7407	. 750	5/1948 - 12/1988	SNOG	94	
BIG MOOSE 3 SE	30		30-0008	43.60	74.87	1760	5/1948 - 12/1988 5/1948 - 12/1988		98 91	
							5/1948 - 12/1988			
BOLIVAR			30-0766	42.07	78.17	1580	5/1948 - 12/1988			
							5/1948 - 12/1988	PP24	55	
							5/1948 - 12/1988			
BOONVILLE & SS			00 05	40 :-	<b>3</b> 5 4 -		5/1948 - 12/1988	SNOG	55	
BOONVILLE 2 SSW	30		30-0785	43.45	75.35	1580				
							10/1949 - 12/1988 10/1949 - 12/1988			
							10/1949 - 12/1988			
BREWERTON LOCK 23	30		30-0870	43.23	76.20	380				
							5/1948 - 12/1988			
BDOCKBOOK & NIM							5/1948 - 12/1988	SNOG	75	
BROCKPORT 2 NW	30		30-0937	43.25	77.97	410				
							2/1950 - 12/1988 2/1950 - 12/1988			
BUFFALO WSFO AP	30	wnd	30-1012	42.93	78.73	710	5/1948 - 12/1988			YES
	_ =				<b></b>	<del>-</del>	1/1922 - 12/1988			. = =
							1/1922 - 12/1988	SNOF		
							1/1922 - 12/1988			
CAMDEN			20	40.00	76 77		1/1979 - 12/1988			
CAMDEN			30-1110	43.33	75.75	510	5/1948 - 12/1988 5/1948 - 12/1988			
							5/1948 - 12/1988 5/1948 - 12/1988			
CANANDAIGUA 3 S	30		30-1152	42.85	77.28	720	5/1948 - 12/1988	PP24	99	
							5/1948 - 12/1988			
CANDOR			30-1168	42.23	76.35	900	5/1948 - 12/1988	PP24		
							5/1948 - 12/1988			
							5/1948 - 12/1988	ZNŌĞ	95	

041/75		US STATIONS, LAKE O	NTARIO DRAINAGE BASIN
CANTON	30	30-1185 44.58 75.17 41	
			1/1922 - +2/1988 PP01 94
CAYUGA LOCK 1			1/1922 - 12/1988 SNOF 07
DATE DOCK T	30	30-1265 42.95 76.73 38	1/1922 - 12/1988 SNOG 96
			5/1948 - 12/1988 PP01 88
CLYDE LOCK 26		•	5/1948 - 12/1988 SNOF 90
OCIDE LOCK 26	30	30-1580 43.07 75.83 390	5/1948 - 12/1988 SNOG 50
			5/1948 - 12/1988 PP24 99
COLTON 2 N		30-1664 44 50 7	5/1948 - 11/1988 SNOG 59
		30-1664 44.58 74.95 580	5/1948 - 12/1987 PP24 00
CORTLAND	30		5/1948 - 10/1987 SNOF 45 5/1948 - 10/1987 SNOG 46
	30	30-1799 42.60 76.18 1130	5/1948 - 12/1988 PP24 9.9
DANSVILLE			5/1948 - 12/1988 SNOE 00
	30	30-1974 42.57 77.70 690	5/1948 - 12/1988 SNOG 99 10/1941 - 12/1988 PP24 84
DANGUM			10/1941 - 12/1988 SNOF 84
DANSVILLE CAA AIR	PORT	30-1979 42.58 77.72 650	10/1941 - 12/1988 SNOG 84
		10.00 77.72 650	5/1948 - 12/1988 PP01 100 5/1948 - 12/1953 PP24 99
EDANISI			5/1948 - 12/1953 PP24 99 5/1948 - 12/1953 SNOF 96
FRANKLINVILLE 1 SS	W 30	30-3025 42.33 78.47 1580	5/1948 - 12/1953 SNOG 05
		10.00 70.47 7580	7/1949 - 12/1988 PP24 95
FREEVILLE 2 NE	30	30-3050 42 52 75 25	7/1949 - 12/1988 SNOG 02
		30-3050 42.53 76.32 1080	6/1948 - 11/1988 PP24 03
FRIENDSHIP 7 SW	30		6/1948 - 11/1988 SNOF 93 6/1948 - 11/1988 SNOG 93
	30	30-3065 42.13 78.23 1640	1/1969 - 12/1988 PP24 90
GANNETT HILL			1/1969 - 12/1988 SNOE 90
The state of the s		30-3124 42.70 77.40 1950	1/1969 - 12/1988 SNOG 99 7/1971 - 12/1988 PP24 95
GENEVA BESEARS			7/1971 - 12/1988 SNOE 00
GENEVA RESEARCH F	ARM 30	30-3184 42.88 77.03 720	7/1971 - 12/1988 SNOG 83
		- 1	5/1968 - 12/1988 PP01 95 1/1969 - 12/1988 PP24 99
GOUVERNEUR			1/1969 - 12/1988 SNOE 100
	30	30-3346 44.33 75.48 460	1/1969 - 12/1988 SNOG 99
CDISSION			5/1948 - 12/1988 SNOE 00
GRIFFISS FIELD	30	30-3507 43.23 75.42 490	5/1948 - 12/1988 SNOG 80
			6/1961 - 12/1988 PP24 99 6/1961 - 12/1988 SNOF 99
HASKINVILLE		30-3722 42.42 77.57 1620	6/1961 - 12/1988 SNOG 05
		00 0722 42.42 77.57 1620	5/1948 - 12/1988 PP24 97
HECTOR		20.2725	5/1948 - 12/1988 SNOF 97 5/1948 - 12/1988 SNOG 97
		30-3766 42.50 76.88 780	5/1967 - 12/1988 PP24 9.6
HEMLOCK			5/1967 - 12/1988 SNOF 90
	30	30-3773 42.78 77.62 900	5/1967 - 12/1988 SNOG 86 1/1926 - 12/1988 PP24 98
HIGHMARKET			1/1926 - 11/1988 SNOF 94
GIMAAREI	30	30-3851 43.57 75.52 1760	1/1926 - 11/1988 SNOG 83
			5/1948 - 12/1988 PP24 100
HINCKLEY			5/1948 - 12/1988 SNOF 93
		30-3889 43.32 75.12 1190	5/1948 - 12/1988 SNOG 58 5/1948 - 12/1988 PP24 97
HORNELL ALLONS			5/1948 - 12/1988 SNOF 93
HORNELL ALMOND DAM	30	30-3983 42.35 77.70 1330	5/1948 - 12/1988 SNOG 60
			211950 - 1211000
ITHACA CORNELL UNIV			2/1954 - 12/1988 SNOF 97
THE CONNECT DAILY	30	30-4174 42.45 76.45 960	2/1954 - 12/1988 SNOG 97
			1/1926 - 12/1988 PP24 9.0
LEWISTON 3 SE			2/1926 - 12/1988 SNOF 05
11151 ON 2 2E		30-4717 43.13 78.97 630	3/1926 - 12/1988 SNOG 97
LOOKE		1	1/1987 - 12/1988 SNOF 90
LOCKE 2 W	30	30:4836 42.57 76 17	1/1987 - 12/1988 SNDG 98
			5/1948 - 12/1988 PP24 99 5/1948 - 11/1988 SNOF 45
			5/1948 - 11/1988 SNOF 45 5/1948 - 11/1988 SNOG 38
			56

			ALIO DI INITAGE DAGI	1.4		
LOCKPORT 2 NE	30	30-4844 43.18 78.65 520	1/1926 - 12/1988	PP24	4 98	
LOCKPORT 4 NE	3.0	30-4849 43.20 78.63 440 30-4912 43.80 75.48 860	1/1926 - 12/1988	SNOC	98	
<b></b>	•	30-4643 43.20 76.63 440	6/1961 - 12/1988	PP24	4 99	
			6/1961 - 12/1968	SNOT	99	
LOWVILLE	30	30-4912 43 80 75 48 860	3/1987 - 12/1988	SIYUG BB01	99	
		4072 42.00 ,70.40 000	1/1926 - 12/1988	PD2/	1 99	
			1/1926 - 12/1988	SNOF	99	
LYONS FALLS	30	30-4944 43.62 75.37 800	5/1948 - 12/1988	PP24	97	
****		30-4944 43.62 75.37 800 30-4952 43.07 77.30 470	5/1948 - 12/1988	SNOF	92	
MACEDON		30-4952 43.07 77.30 470	5/1948 - 12/1988	PP24	72	
			5/1948 - 12/1988	SNOF	56	
*****		30-5171 43.00 76.77 400	5/1948 - 12/1988	SNOG	42	
MAYS POINT LOCK 25	30	30-5171 43.00 76.77 400	5/1948 - 12/1988	PP24	98	
			5/1948 - 11/1988	SNOF	76	
MOUNT MODDLE SW	• •		5/1948 - 11/1988	SNOG	59	
MODITI MORRIS 2 W	30	30-5597 42.73 77.90 880	6/1950 - 12/1988	PP01	93	
		30-5597 42.73 77.90 880 30-5679 43.05 77.08 430 30-5751 43.22 75.65 400	8/1948 - 12/1988	PP24	97	
			8/1948 - 11/1988	SNOF	92	
NEWARK	3.0	20-5570 42.05 77.00 400	8/1948-12/1988	SNOG	95	
	30	30-36/9 43.05 //.08 430	5/1948 - 12/1988	PP24	98	
			5/1948 - 12/1988	SNOF	68	
NEW LONDON LOCK 22	3.0	30-5751 43 33 75 65 400	5/1948 - 11/1988	SNOG	51	
	30	30-3751 43.22 75.65 400	5/1948 - 12/1988	PP24	99	
			5/1948 - 11/1988	SNOF	76	
NORFOLK	30	30-5869 44.80 75.00 230	5/1940 - 11/1900 5/1948 - 19/1999	21/00	58	
		20 0000 44.00 75.00 250	5/10/0 - 12/1900	PPZ4	99	
		30-5869 44.80 75.00 230 30-6047 43.08 78.75 6080	5/1940 - 12/1900	SNOC	96 80	
NORTH TONAWANDA		30-6047 43.08 78.75 6080	9/1982 - 12/1988	DD24	98	
		12,00 10,10 0000	9/1982 - 12/1988	SNOE	98	
			9/1982 - 12/1988	SNOG	98	
OGDENSBURG HOSP 3 NE	30	30-6164 44.73 75.45 280	1/1926 - 12/1988	PP24	96	
			1/1926 - 12/1988	SNOF	85	
<b>.</b>			1/1926 - 12/1988 1/1926 - 12/1988	SNOG	72	
OLD FORGE	30	30-6184 43.70 74.98 1720	5/1948 - 12/1988	PP01	93	
			5/1948 - 12/1988	PP24	94	
			9/1948 - 12/1988	SNOF	90	
DEWECO ELOT		30-6314 43.47 76.50 350	9/1948 - 12/1988	SNOG	89	
USHEGO EAST	30	30-6314 43.47 76.50 350	5/1948 - 12/1988	PP01	95	
			17.020 12.1300	F F & 4	22	
			1/1926 - 12/1988			
PAVILION	3.0	30-6464 42.88 78.03 940	1/1926 - 12/1988	SNOG	98	
TATION	30	30-6464 42.88 78.03 940	11/1956 - 12/1988	PP01	91	
			311330 - 1211300	FF24	33	
			9/1956 - 12/1988			
PENN YAN 8 W	30	30-6517 42.67 77.18 1000	9/1956 - 12/1988	SNOG	99	
		42.07 77.10 7000	6/1984 - 12/1988		93	
			6/1984 - 12/1988	SNOF SNOG	98 92	
PORTAGEVILLE	30	30-6745 42.57 78.05 1120	6/1956 - 12/1988	DD24	97	
			6/1956 - 12/1988		74	
			6/1956 - 12/1988		74	
PRATTSBURG 2 NW		30-6831 42.53 77.30 1940	/1948-10/1986			
			/1948-10/1986			
DD ATTORUS C			/1948-10/1986			
PRATTSBURG		30-6833 42.52 77.27 1470	1/1988 - 12/1986			
			1/1988 - 12/1986	SNOF	100	
DULACAL			1/1988 - 12/1986	SNOG	100	
PULASKI		30-6867 43.57 76.13 360	5/1948 - 7/1949	PP01	97	
•				PP24	60	
				SNOF		
RECTORS CORNERS		20.5055 40 75 75 75	5/1948 - 12/1988	SNOG		
TO SOUNERS		30-6965 43.75 75.58 1810				
			1/1987-12/1988	SNOF		
ROCHESTER WB AP	30 wad	30-7167 43.12 77.67 550	1/1987-12/1988	SNOG	99	
	- mil	00 7107 43.12 77.07 550				YES
				PP24	99	
				SNOF	99	
				SNOG	99	
RUSHFORD	30	30-7329 42.40 78.25 1500		PP24	74 96	
			4/1954 - 11/1988		89	
			4/1954 - 11/1988		73	
			3.00. 1171900	J. 10 G	, ,	

CKANE. ~~		WHOMA, DAKE ON	TAHIO DHAINAGE BASI	N		
SKANEATELES	30	30-7780 42.95 76.43 880	F/40.40			
		14.45 660	5/1948 - 12/1988	PP24	99	
SODUS 2 SSW			5/1948 - 12/1988	SNOF	99	
20202 5 22 M	30	30-7842 43.22 77.07 440	5/1948 - 12/1988	SNOG	99	
		= *****	5/1948 - 12/1988	PP24	97	
STILL WATER DESERVOIS		30-8248 43.88 75.03 1700	5/1948 - 12/1988	SNOF	91	
WESERAOIH	30	30-8248 43.88 75.03 1700	5/1946 - 12/1988	SNOG	92	
		•	5/1940 - 12/1988	PP01	97	
			5/1948 - 12/1988 5/1948 - 12/1988			
STONY POINT 2 F			5/1948 - 12/1988	SNOC	93	
SYRACUSE WB AP	2.0	wnd 30-8290 43.83 76.27 260	4/1978 - 12/1988	DDM	64	
	30	wnd 30-8290 43.83 76.27 260 30-8383 43.12 76.12 420	5/1948 - 12/1988	PP01	100	V=0
			1/1922 - 12/1988	PP24	99	YES
			1/1922 - 12/1988	SNOF	00	
<b></b>						
THENTON FALLS	30	30-8578 43.27 75.15 800	1/1979 - 12/1988	SNWE	76	
		00 0070 43.27 75.15 800	5/1948 - 12/1988	PP24	9.8	
				SNOF	6.8	
UTICA CAA AP	3.0	30-8737 43 15 75 20 710	5/1948 - 11/1988	SNOG	53	
		30-8737 43.15 75.38 710	1/1951 - 10/1952	PP01	92	
•			12/1950 - 12/1988	PP24	96	
UTICA 2 SE			12/1950 - 12/1988	SNOF	96	
011CA 2 3E		30-8739 43.08 75.18 500	12/1950 - 12/1988	SNOG	96	
		300	10/1952 - 12/1988	PP01	88	
			8/1948 - 12/1988 8/1948 - 12/1988	PP24	89	
VICTOR			8/1948 - 12/1988	SNOF	87	
		30-8839 42.98 77.42 640	5/1948 - 12/1989	SNOG	87	
•			5/1948 - 12/1988	PP01	99	
			5/10/8 - 10/1000			
WANAKENA HANGER SCH	3.0	30-8944 44.15 74.90 1510	6/1948 - 12/1988	SNOG	8 8	
2011	30	30-8944 44.15 74.90 1510	5/1948 - 12/1988	PP01	92	
			1/1926 - 12/1988	PP24	99	
			1/1926 - 12/1988		99	
WARSAW 5 SW		30-8962 42.50 70.00			98	
		30-8962 42.68 78.20 1720	10/1978 - 5/1981	PP01	56	
			11/1952 - 12/1988	PP24	93	
WATERIAL			11/1952 - 12/1988	SNOF	91	
WATERLOO	30	30-8987 42.90 76.87 450	12/1952 - 12/1988	SNOG	91	
		-1 000, 42,50 70,87 450	5/1948 - 12/1988	PP24	98	
			5/1948 - 12/1988	SNOF	92	
WATERTOWN	30	30-9000 43.97 75.87 500	5/1948 - 11/1988	SNOG 6	64	
		7 7 7 2 2 7 2 7 2 7 2 7 2 7 2 7 2 7 2 7		PP01 9	97	
			1/1926 - 12/1988	PP24	99	
WATERTOWN FAA AP			1/1926 - 12/1988	SNOF 9	97	
THE PAR AP		30-9005 44.00 76.02 320	1/1926 - 12/1988 : 5/1949 - 4/1951	SNOG 9	90	
			5/1949 - 12/1988	PP01 8		ES
					34	
WELLESLEY ISLAND			E (4.0.40		5	
		30-9055 44.30 76.03 280	744.07		15	
			7/4 / 7 / 4 / 4 / 4 / 4 / 4 / 4 / 4 / 4	PP24 9 SNOF <sup>*</sup> 9		
WELLSVILLE 3	0	30-0070	7/1974 - 12/1988 - 5	SNOG 9		
-		30-9072 42.12 77.95 1510	12/1955 - 12/1988	PP01 9		
			6/1956 - 12/1988	PP24 9		
			6/1956 - 12/1988 9	NOF 9		
WELLSVILLE 4 NNW		30-9076 42.17 77.98 1460	6/1956 - 12/1988 S	NOG 9		
		20 3070 42.17 77.98 1460	9/1975 - 12/1988	PP24 9	5	
William -			9/1975 - 12/1988 5	NOF 9:	3	
WHITESVILLE 3	٥	30-9425 42.03 77.77 1720	9/1975 - 12/1988 S	NOG 9:	3	
		12.00 17.77 1720	2/1954 - 12/1988	PP24 99	9	
WILSON 2 NE			2/1954 - 12/1988 S	NOF 9		
HILDOR Z NE		30-9507 43,32 78.80 270	2/1954 - 12/1988 S.	NOG 99	•	
		10,00 270	P 14 A 4A	P24 97		
WISCOY 1 E			5/1948 - 11/1988 S	NOF 69		
		30-9533 42.50 78.07 1140	EMOAR ABOVE	NOG 65	-	
			E14 0 10	P24 93		
WOLCOTT			Eta A to	NOF 80		
·		30-9544 43.22 76.82 370	Present and a service of	NOG 75 PP24 90		
			EIG DAG . A	P24 90 NOF 75		
			£ 10 0 10	VOG 54		

PENNSYLVANIA							
GALETON	30	36-3130	41.73	77.63 1370	5/1948 - 12/1988	PP24	99
					5/1948 - 12/1988	SNOF	99
					5/1948 - 12/1988	SNOG	98
RAYMOND	30	36-7310	41.87	77.87 2200	5/1948 - 12/1988	PP01	90
					6/1948 - 12/1988	PP24	90
				•	2/1954 - 12/1988	SNOF	80
				•	2/1954 - 12/1988	SNOG	84
SABINSVILLE 3 SE		36-7730	41.83	77.47 200	10/1951 - 1/1952	PP01	31
					12/1969 -12/1988	PP24	98
					4/1970 -11/1988	SNOF	76
					3/1970 - 12/1988	SNOG	96
WESTFIELD 5 S		36-9490	41.98	77.57 1880	11/1981 - 12/1988	PP01	73
					10/1981 - 10/1988	PP24	78
					10/1981 - 10/1988	SNOF	71
110750					10/1981 - 10/1988	SNOG	65

#### NOTES

- Most information from the Climatic Data files (CNIFINDX) for the States of New York and Pennsylvania obtained from the Office of Hydrology, National Weather Service, NOAA, Silver Spring, Maryland.
- Records of daily precipitation values (PP24) for all listed stations, for the period from January 1955
  through 1990, were obtained from the files of the NOAA Library, Rockville, Maryland and are stored
  on Hydex's computer system.
- Records of snowfall (SNOF), snow on the ground (SNOG) and hourly precipitation data (PP01) and snow water equivalent (SNWE) are available at the NOAA Library, Rockville, Maryland but have not been transfered to Hydex files.

#### FOOTNOTES

- 1/ For those stations marked 30, thirty-year normals (annual, October-April and May-September), based on the period 1961-1990, have been computed. Missing data for these stations have been estimated from nearby stations.
- 2/ Exposure of proipitation gage as defined by Brown and Peck (AGU 1962). WP Well protected. PRO - Protected. FWP - Fairly well protected. MW - Moderately Windy. WND - Windy, VWND - Very windy. OPRO = Over protected.
- 3/ Records for years 1955-1988 were obtained from the CD-R0M files (Climatedata) at NOAA Library, Rockville, Maryland. Records for years 1989 and 1990 were processed from Climatic data publicationas and are included in Hydex files.
- 4 Overall percentage of non-missing data for period of record indicated in previous column.

Hydex, MAY 1991

3.5 3.5 4. 21.5 12. 12. 12. 12. 12. 12. 12. 12. 12. 12.	NAN	14 14 18	MAR	604	ξ		BEAVI	ER FAL	- 6	ÌN.	۳۲		ATTAC	ATTACHMENT	N
5.54 2.15 2.59 160 2.29 3.67 2.30 5.83 1.90 0.90 2.917 5.55 1.28 2.10 3.12 3.66 1.85 3.41 2.15 2.965 16.86 6.31 1.60 3.13 4.63 6.09 5.74 4.67 3.24 2.94 1.30 37.24 10.99 6.31 1.60 3.13 4.63 6.09 5.74 4.67 3.24 2.94 1.30 37.24 10.99 6.33 2.10 4.25 4.25 6.09 5.74 4.67 3.24 2.94 1.30 37.24 10.99 6.34 2.15 2.15 3.99 2.24 3.56 1.70 3.22 3.00 2.63 3.423 1.77 6.15 2.17 2.13 3.18 1.89 2.95 5.43 5.40 5.25 1.75 30.67 2.25 1.94 5.15 2.77 2.28 1.45 5.19 6.34 5.44 2.56 1.42 2.46 37.64 18.81 5.27 2.16 3.50 1.44 2.21 3.22 0.79 1.78 2.97 2.82 3.77 1.14 3.37 0.97 5.32 3.78 3.90 5.16 1.59 34.04 16.38 5.27 2.16 3.50 1.14 2.21 3.22 0.79 1.78 2.97 2.82 3.43 16.53 3.27 2.40 3.70 2.10 3.70 3.13 1.30 1.82 4.89 2.87 3.80 2.10 3.70 3.13 1.30 1.82 4.89 2.87 3.80 2.40 2.80 3.77 2.16 3.80 3.70 3.70 3.18 3.90 2.24 2.80 3.77 3.80 3.90 2.10 3.70 3.13 1.30 1.82 4.89 2.87 3.80 3.80 4.26 3.77 4.48 3.87 5.27 3.78 3.90 2.24 2.80 3.77 4.48 3.87 5.77 3.83 3.80 4.26 3.77 3.80 3.70 3.20 3.70 3.70 3.70 3.70 3.70 3.70 3.70 3.7	-		, , ,	۲ ٔ			) ] ]	<b>A</b> U6			<u></u>	DEC	ANNUAL (	OCT-APR I	1AY-SEP
2.56 2.30 3.11 182 2.10 312 386 1.85 341 2.15 29.65 16.86 0.31 1.28 3.22 4.70 3.26 0.81 442 1.09 2.42 1.98 27.45 1.296 0.31 1.28 3.22 4.70 5.26 0.81 442 1.09 2.42 1.98 27.45 1.296 0.31 1.80 2.95 5.43 2.40 5.24 1.30 37.24 1.099 1.77 2.11 3.18 1.89 2.95 5.43 2.40 5.24 3.70 4.38 39.46 1.777 2.11 3.18 1.89 2.95 5.43 2.40 5.24 3.70 2.33 37.24 10.99 1.77 2.11 3.18 1.89 2.95 5.43 2.40 5.24 3.70 2.33 3.42 3.17 2.25 1.45 5.19 6.34 5.44 2.56 1.42 2.46 37.64 1.77 2.03 3.47 2.82 1.45 5.19 6.34 5.44 2.56 1.42 2.46 37.64 1.88 1.30 2.77 1.14 3.70 1.14 2.14 2.18 2.97 2.10 3.70 3.13 1.30 1.82 4.89 2.8.77 1.14 3.70 1.14 2.10 2.10 3.20 3.00 2.14 2.24 3.70 1.18 2.10 3.20 3.14 2.21 3.22 3.70 3.13 1.30 1.82 4.89 2.8.77 1.14 3.70 1.20 2.10 3.70 3.13 1.30 1.82 4.89 2.8.73 1.82 9.7 2.40 2.32 2.94 2.32 2.14 2.18 2.19 2.10 3.70 3.13 1.30 1.82 4.89 2.8.73 1.82 9.7 2.40 2.32 2.94 2.25 2.10 2.10 2.00 3.25 2.94 2.25 2.10 2.10 2.00 3.25 3.70 3.13 1.30 1.82 4.89 2.8.73 1.20 1.42 2.46 5.12 6.25 2.11 2.41 2.18 2.27 3.68 3.57 3.67 9.50 2.44 2.56 2.32 2.40 2.80 1.75 2.20 3.70 3.33 3.40 4.61 6.93 3.71 3.08 3.56 5.13 4.130 2.44 0.30 3.33 3.44 3.46 5.12 6.25 2.11 2.41 2.18 2.24 2.50 3.90 3.66 1.30 2.54 4.71 4.70 3.03 3.40 4.61 6.93 3.71 3.08 3.56 5.13 4.130 2.44 0.30 3.33 3.44 3.46 1.69 3.71 3.29 3.56 5.13 4.130 2.44 0.30 3.33 3.44 3.46 1.69 3.71 3.29 3.50 3.50 3.85 2.53 2.20 3.30 3.30 3.30 3.30 3.30 3.30 3.3	- 0		5.54	<del>-</del> , 1	2.59		2.29		0	5.83	1.90	06.0	29.17		
1.32 1.28 3.22 4.70 3.26 0.81 442 1.09 2.42 1.98 27.45 1.296 0.31 1.60 3.11 4.63 5.24 4.70 3.26 0.81 442 1.09 2.42 1.99 2.74 5.10 3.18 1.80 3.29 2.95 5.43 2.40 5.24 3.64 1.30 3.724 1.099 1.77 2.11 3.18 1.82 2.95 5.43 2.40 5.24 3.04 3.8 3.42 3.17 77 2.11 3.18 1.82 2.95 5.43 2.40 5.24 3.06 1.42 2.15 3.06 7.24 5.17 3.06 1.10 3.14 5.12 5.12 5.25 2.20 1.69 3.28 1.52 1.05 3.43 1.77 3.25 3.12 2.31 5.88 0.94 0.38 5.12 2.65 3.43 1.77 3.05 2.77 3.25 2.13 5.88 0.94 0.38 5.12 2.65 3.43 1.75 1.03 3.47 3.25 2.15 5.88 0.94 0.38 5.16 1.59 3.40 1.65 3.3 3.2 2.77 3.25 2.15 5.88 0.94 0.38 5.16 1.89 2.77 3.10 1.20 3.70 1.10 2.14 3.37 0.97 5.32 3.78 3.90 5.16 1.89 2.77 3.10 1.20 3.70 1.10 2.10 3.70 1.10 2.10 3.70 3.10 3.00 3.00 3.00 3.00 3.00 3.00 3.0	Ņ.		2.56	W I	3.1		2.10		S	1.85	3.41	2.15	29.65	16.86	
0.31 1.60 3.13 4.63 6.09 5.74 4.67 324 2.94 130 37.24 10.99 0.37 2.11 5.11 5.18 1.89 2.95 5.43 2.40 5.24 3.70 4.38 35.24 10.99 0.37 2.11 5.18 1.89 2.29 5.43 2.40 5.24 3.70 4.38 39.46 17.77 0.35 2.30 4.25 4.25 1.77 2.11 5.18 1.89 2.24 3.56 1.70 3.22 3.00 2.63 34.23 1.77 1.34 5.17 2.13 2.17 2.19 5.19 2.24 3.56 1.70 3.22 3.00 2.63 34.23 1.77 1.35 2.77 2.82 1.45 5.19 6.34 5.44 2.56 1.42 2.46 3.76 4 18.81 1.35 2.77 2.16 3.50 1.42 2.37 2.32 0.79 1.78 2.37 2.37 2.37 2.37 2.37 2.37 2.37 2.37		<u>~</u> [	1.52	Ų,	3.22		3.26		$\sim$	1 09	2.42	1.98	27.45	12.96	16.41
1.77 1.1 3.18 1.89 2.95 5.43 2.40 5.24 3.70 4.38 39.46 17.77 1.1 3.18 1.89 2.95 5.43 2.40 5.24 3.70 4.38 39.46 17.77 1.1 3.13 1.81 1.89 2.95 5.43 2.40 5.24 3.70 2.63 3.0.67 2.25 1.94 5.13 2.73 2.73 2.25 2.20 1.05 3.22 3.0.0 2.63 3.43 1.653 3.0.0 2.77 3.25 3.32 2.31 5.88 0.94 0.38 5.51 2.66 34.34 1.653 3.70 2.77 3.25 3.32 2.31 5.88 0.94 0.38 5.51 2.66 34.34 1.653 0.35 2.77 3.25 3.78 3.90 5.16 1.59 2.0.7 3.13 1.30 1.82 4.89 2.8.7 3 1.8.1 1.30 1.32 2.74 2.88 1.76 3.79 5.16 2.88 3.98 4.52 1.35 3.32 7 14.96 2.32 2.74 2.86 1.55 1.92 2.10 3.70 3.13 1.30 1.82 4.89 2.8.7 3 1.20 1.47 4.46 5.12 6.21 2.11 2.18 2.27 3.67 9 2.27 8 1.55 1.92 2.10 3.70 3.13 1.30 1.82 4.89 2.8.7 1.496 2.10 3.70 3.13 1.30 1.82 4.89 2.8.7 1.496 3.70 2.10 2.18 3.87 5.37 3.79 5.16 43.24 1.8.20 1.97 1.20 1.97 1.54 3.88 2.22 4.17 3.70 3.63 1.25 3.52 2.69 3.95 0.946 3.70 3.08 2.27 3.8 3.8 4.52 1.3 2.41 2.18 2.27 3.67 9 2.27 3.8 2.20 4.17 3.70 3.63 1.25 3.2 2.69 3.95 0.946 3.70 3.08 2.20 3.70 3.08 2.20 3.70 3.08 3.70 3.70 3.70 3.70 3.70 3.70 3.70 3.70	_ (	, K	٠. د د د د د د	٠ ب	5.13		60.9		_	3.24	2.94	1.30	37.24	10.99	24.26
1.03 2.20 4.25 4.52 2.23 2.20 169 3.28 1.55 1.75 3.067 22.52 1.03 3.47 2.89 2.24 3.56 1.70 3.22 2.46 34.24 16.53 3.05 2.77 3.25 3.32 2.31 5.88 0.94 0.38 5.51 2.66 34.34 16.53 3.05 2.77 3.25 3.32 2.31 5.88 0.94 0.38 5.51 2.66 34.34 16.53 3.27 2.16 3.50 1.14 2.21 3.22 0.79 1.78 2.97 2.82 2.77 1.14 3.37 0.97 5.32 3.78 3.99 2.82 2.78 3.90 5.16 1.59 3.404 16.53 0.32 2.94 2.88 1.76 3.79 5.16 2.88 3.98 4.52 1.35 3.32.7 14.96 2.25 0.87 1.16 3.37 0.97 5.16 2.88 3.98 4.52 1.35 3.32.7 14.96 2.21 4.13 3.41 16.3 2.01 4.20 4.64 4.83 4.11 36.31 17.20 1.91 2.78 3.38 2.22 4.17 3.70 3.63 1.35 3.22 2.69 3.57 3.04 16.38 2.04 4.04 4.04 4.04 4.04 4.04 4.04 4.04	7 2			7.1.	5 2 3 1		2.95		$\circ$	5.24	3.70	4.38	39.46	17.77	15.85
1.03 2.47 2.82 1.45 5.19 6.34 5.40 2.65 34.23 17.74 3.05 2.65 34.74 2.82 1.93 2.47 2.82 1.45 5.19 6.34 5.40 2.65 34.24 16.53 3.02 2.77 2.82 1.45 5.19 6.34 5.40 2.65 1.42 2.66 34.74 16.53 3.72 2.16 3.50 1.14 2.21 3.22 0.79 1.78 2.97 2.82 3.779 1.791 1.35 2.77 1.14 3.37 0.97 5.32 3.78 3.90 5.16 1.59 34.04 16.38 0.32 2.94 2.88 1.76 3.70 3.13 1.30 1.82 4.89 2.87.7 14.96 2.24 2.88 1.76 3.70 3.13 1.30 1.82 4.89 2.87.7 14.96 2.24 2.88 1.76 3.40 1.20 2.40 2.24 4.85 2.10 2.41 1.52 2.10 2.74 4.85 2.11 2.41 2.18 2.27 3.68 3.57 3.67 9 2.78 1.90 2.24 4.85 3.77 4.48 3.87 5.37 3.79 5.16 4.32 4.11 2.64 1.54 3.20 2.94 3.87 5.37 3.70 3.81 3.22 2.99 3.50 3.77 4.48 3.87 5.37 3.79 5.16 4.11 2.8 2.27 3.88 3.85 4.26 3.77 4.48 3.87 5.37 3.98 1.30 2.44 1.30 2.26 3.59 3.66 3.15 2.81 4.11 1.51 5.27 3.71 3.98 1.20 2.24 4.11 2.8 2.27 3.88 2.86 4.61 2.13 2.24 4.11 2.8 2.87 3.88 4.28 6.06 1.30 2.24 4.11 2.66 3.92 3.66 3.15 2.81 4.11 1.26 1.30 2.84 4.61 2.15 2.89 3.10 3.88 4.28 6.06 1.30 2.24 4.11 2.66 3.28 3.28 6.46 1.20 3.08 3.20 3.88 3.28 3.48 4.80 4.61 2.15 3.37 3.88 3.88 4.88 4.88 5.18 3.10 3.88 3.88 4.88 5.18 3.10 3.88 3.88 3.88 3.89 3.99 3.88 3.88 3.88	רכ	7 (	0.0	2.30	4.23 5.14		2.23		On .	3.28	1.55	1.75	30.67	22.52	14.89
3.05 3.77 2.62 1.45 3.19 634 544 2.56 1.42 2.46 37.64 18.81 3.05 2.77 2.62 3.32 2.31 5.88 0.94 0.38 5.51 2.66 34.34 16.53 3.02 2.77 1.14 3.37 0.97 5.32 3.78 3.90 5.16 1.59 34.04 16.38 2.27 1.14 3.37 0.97 5.32 3.78 3.90 5.16 1.59 34.04 16.38 2.30 2.34 1.15 3.31 17.91 2.52 0.87 1.55 1.92 2.10 3.70 3.13 1.30 1.82 4.89 2.8.7 14.96 2.32 2.34 4.15 3.35 1.35 3.32 1.496 2.32 2.34 4.15 3.38 2.22 4.10 3.70 3.13 1.30 1.82 4.89 3.81 4.11 1.63 2.37 1.496 2.37 3.86 4.26 3.77 4.48 3.87 5.37 3.79 5.16 43.24 18.20 1.91 2.78 3.86 4.26 3.77 4.48 3.87 5.37 3.79 5.16 43.24 18.20 3.75 2.30 4.61 6.82 6.07 2.52 1.90 2.55 4.25 4.75 4.59 2.40 3.75 2.69 3.95 0.29 4.00 3.05 3.99 3.66 3.15 2.81 4.11 1.51 5.27 3.71 3.98 1.22 2.69 3.95 0.20 4.00 3.05 3.99 3.66 3.15 2.81 4.11 1.51 5.27 3.71 3.98 1.25 2.69 3.95 0.09 3.22 2.69 3.95 3.66 3.15 2.81 4.11 1.51 5.27 3.71 3.98 1.25 2.69 3.95 3.66 3.15 2.81 4.11 1.51 5.27 3.71 3.98 1.25 2.69 3.95 3.66 3.15 2.81 4.11 1.51 5.27 3.71 3.98 1.73 2.20 3.20 3.20 3.20 3.20 3.20 3.20 3.2	4 (	25.0	y	0. L	2.73		2.24		0	3.22	3.00	2.63	34.23	17.74	14.22
3.70         2.77         5.25         5.31         5.88         0.94         0.38         5.51         2.66         34.34         16.53           3.27         2.16         5.50         1.14         2.21         5.22         0.79         1.78         2.97         2.82         2.79         1.791           1.35         2.0         1.16         2.21         3.70         3.13         1.30         1.82         28.73         14.96           2.52         0.87         1.52         2.10         3.70         3.13         1.30         1.82         28.73         14.96           2.52         0.87         1.55         2.10         3.70         4.69         28.73         14.96           2.40         2.21         3.41         1.63         2.01         4.20         4.64         4.83         4.11         3.51         1.72           1.91         2.24         4.13         3.41         1.63         2.01         4.20         4.64         4.83         4.11         3.51         1.72           1.91         2.24         4.73         3.70         5.64         4.83         4.11         3.51         4.72         4.72         4.72         4.72	•	7-7-	. U. V	0.0 - 1.0	2.87	A 1	5.19			2.56	1 42	2.46	3764	18.81	21.24
3.27         2.16         5.50         1.14         2.21         3.22         0.79         1.78         2.97         2.87         1.791           2.55         2.77         1.14         3.37         0.97         5.32         3.78         3.90         5.16         1.59         3.404         16.38           2.52         2.78         1.50         1.62         2.01         4.20         4.64         4.89         4.89         2.27         1.49           2.40         2.21         4.13         3.41         1.65         2.01         4.20         4.64         4.89         4.89         4.89         1.72         1.49           2.40         2.21         4.11         1.63         2.01         4.20         4.64         4.89         4.11         1.20         1.89         3.57         3.67         2.78         1.90         5.71         3.69         3.65         3.51         3.27         1.496         2.71         4.64         3.89         3.57         3.67         2.78         1.99         3.67         3.22         2.69         3.57         3.79         3.64         4.82         3.24         4.64         3.83         3.51         3.22         2.69         3.57 <td>•</td> <td>0 0</td> <td>5.U3</td> <td>7.7.7</td> <td>5.25</td> <td>Λı.</td> <td>2.31</td> <td></td> <td></td> <td>0.38</td> <td>5.51</td> <td>2.66</td> <td>34.34</td> <td>16.53</td> <td>15.70</td>	•	0 0	5.U3	7.7.7	5.25	Λı.	2.31			0.38	5.51	2.66	34.34	16.53	15.70
1.55 2.77 1.14 3.57 0.97 5.32 3.78 3.90 5.16 1.59 34.04 16.38 0.32 2.94 2.87 1.92 2.10 3.70 3.13 1.30 1.82 4.89 2.8.73 18.97 0.32 2.94 2.88 1.76 2.24 4.18 2.70 3.70 3.13 1.30 1.82 4.89 2.8.73 1.720 2.24 4.13 4.13 6.12 6.25 2.11 2.41 2.41 2.42 3.88 4.26 4.26 3.77 4.48 3.87 5.37 3.79 5.16 43.24 18.20 3.75 2.30 4.61 6.82 6.07 2.52 1.90 2.55 4.25 4.75 3.79 5.16 43.24 18.20 3.75 2.30 4.61 6.82 6.07 2.52 1.90 2.55 4.25 4.75 4.59 2.69 39.50 2.946 4.00 3.05 3.99 3.66 3.15 2.81 1.51 5.27 3.71 3.08 3.56 3.13 1.30 2.44 3.46 1.69 3.71 3.08 3.56 5.13 41.30 2.47 3.40 1.51 2.20 5.81 4.56 3.22 4.93 4.61 1.51 2.20 3.92 3.66 3.16 3.22 4.93 4.61 1.51 2.20 3.92 3.66 3.16 3.22 4.93 4.61 1.51 2.85 7.35 4.45 6.71 3.29 3.92 3.68 4.61 2.15 1.30 2.87 1.30 2.87 2.69 3.88 4.28 6.06 1.30 2.24 4.71 4 2.40 6.45 2.83 1.26 1.65 2.67 7.72 5.47 4.50 5.59 5.65 3.88 4.28 6.06 1.30 2.24 4.71 4 2.40 6.45 2.83 1.26 1.65 2.67 7.72 5.47 4.50 5.59 5.65 3.08 2.28 1.26 1.12 2.66 1.14 2.94 5.32 2.86 1.64 3.60 3.08 5.25 2.10 1.11 2.66 1.14 2.94 5.32 2.86 1.64 3.60 3.08 5.25 1.11 2.66 1.14 5.24 2.14 4.52 5.26 2.74 4.11 2.61 3.92 1.93 1.33 2.87 2.16 1.11 2.64 3.20 3.08 3.08 9.29 4.32 1.81 3.21 4.89 5.47 5.13 4.71 2.14 1.75 3.726 1.93 1.85 5.27 3.48 1.92 1.61 8.82 2.34 3.10 3.88 9.29 4.32 1.93 1.85 5.27 3.48 1.92 1.61 8.82 2.34 3.10 3.88 9.29 4.32 1.93 3.18 2.31 3.18 3.31 3.21 4.89 5.47 5.33 3.48 6.26 1.60 4.01 1.20 4.3 3.18 2.31 3.18 3.19 2.65 4.47 5.33 3.48 6.26 1.60 4.01 1.20 4.3 3.18 2.31 3.18 3.18 3.18 3.18 3.18 3.18 3.18 3	- '	20.0	5.27	2.16	3.50		2.21			1.78	2.97	2.82	27.79	17.91	10.86
2.52 0.87 1.55 1.92 2.10 3.70 3.13 1.30 1.82 489 28.73 18.97 0.32 2.94 2.88 1.76 3.79 5.16 2.88 3.98 4.52 1.35 33.27 14.96 2.40 2.21 4.13 3.41 1.63 2.01 4.20 4.64 4.83 4.11 36.31 1.720 1.47 446 5.12 6.25 2.11 2.41 2.18 2.27 3.68 3.57 36.79 5.67 9 22.78 1.91 2.78 3.86 4.65 3.77 4.48 3.87 5.37 3.79 5.6 3.95 2.94 1.54 3.38 2.22 4.17 3.70 5.53 3.22 6.9 39.50 2.94 2.95 4.15 4.38 2.22 4.17 3.70 2.55 4.25 4.75 4.59 19.71 2.26 5.61 4.38 3.44 3.46 1.69 3.71 3.08 3.56 5.13 41.30 24.40 3.05 3.99 3.66 3.15 2.81 4.11 1.51 5.27 3.71 39.81 2.3.7 2.78 1.93 1.34 2.85 7.35 4.45 6.07 2.52 1.90 2.55 4.25 4.75 4.51 2.30 1.34 2.85 7.35 4.45 6.16 3.71 3.08 3.56 5.13 41.30 2.44 4.11 1.51 5.27 3.71 39.81 2.3.37 2.78 1.93 1.34 2.85 7.35 4.45 6.11 1.51 5.27 3.71 39.81 2.3.37 2.45 6.10 1.20 1.30 2.55 5.53 4.41 1.51 2.66 1.14 2.94 5.0 2.94 4.50 2.95 5.65 4.57 5 2.16 1.11 2.66 1.14 2.94 5.32 2.86 1.64 3.80 3.08 5 2.084 1.35 2.16 1.11 2.66 1.14 2.94 5.2 2.14 4.12 2.14 1.75 3.72 6 39.85 2.15 3.13 4.13 2.87 3.16 2.12 4.89 4.57 5 1.14 1.75 3.72 6 39.28 2.08 2.25 2.25 2.25 2.25 2.25 2.25 2.25 2.2		2.80	1.55	2.77	<u>-</u> - 4		0.97			3.90	5.16		34.04	16.38	14.58
0.32 2.94 2.88 1.76 3.79 5.16 2.88 3.98 4.52 1.35 33.27 14.96 2.40 2.21 4.13 3.41 1.63 2.01 4.20 4.64 4.83 4.11 36.31 17.20 1.47 4.46 5.12 6.25 2.11 2.41 2.18 2.27 3.68 3.57 36.79 2.2.78 1.91 2.78 3.38 2.22 4.10 2.41 2.18 2.27 3.68 3.57 36.79 2.2.78 2.46 1.54 3.38 2.22 4.10 2.52 1.90 2.55 4.25 4.75 45.92 19.71 2.26 5.61 4.38 3.44 3.46 1.69 3.71 3.08 3.56 5.13 41.30 2.44 0.0 3.05 3.99 3.66 3.15 2.81 4.11 1.51 5.27 3.71 3.98 1 23.37 2.40 4.40 2.05 3.99 3.66 3.15 2.81 4.11 1.51 5.27 3.71 3.98 1 23.37 2.26 5.61 4.38 7.35 4.45 6.71 3.29 3.92 3.68 4.461 2.151 2.26 5.61 4.38 2.47 2.85 7.35 4.45 6.71 3.29 3.92 3.68 4.461 2.151 2.27 8 1.93 1.34 2.85 7.35 4.45 6.71 3.29 3.92 3.68 4.461 2.151 2.69 5.82 7.73 2.66 3.84 4.20 5.59 5.65 4.47 4.45 2.83 1.36 2.84 7.34 2.85 5.15 3.13 4.92 2.66 3.92 8 20.84 1.35 2.16 1.11 2.66 1.14 2.94 5.35 2.44 1.17 2.64 3.90 3.88 2.28 2.16 1.11 0.91 5.85 5.15 3.13 4.92 2.66 3.92 8 20.82 2.65 2.71 2.14 4.52 2.54 4.11 2.61 3.92 7.13 1.13 2.87 2.14 4.52 2.14 4.52 2.54 4.11 2.61 3.92 4.43 1.92 1.61 8.82 2.34 3.10 2.91 4.52 3.53 2.89 1.81 3.21 4.89 5.47 3.22 2.59 1.00 2.91 4.52 3.53 3.91 8 2.31 3.15 2.14 4.86 2.19 2.44 3.46 5.65 4.46 1.57 3.43 3.18 2.31 3.18 3.14 4.86 2.19 5.04 3.17 3.43 3.18 2.13 3.18 2.14 4.86 2.19 5.04 3.17 3.18 4.80 3.19 2.18 2.11 4.86 2.19 5.19 4.05 3.19 4.05 3.19 4.05 3.19 2.10 3.11 4.86 2.19 5.04 3.17 3.42 3.18 4.85 2.19 3.18 2.11 4.86 2.19 5.04 3.17 3.42 3.13 3.18 2.13 3.18 2.11 4.86 2.19 5.04 3.17 3.43 3.18 3.17 3.42 3.17 3.43 3.18 2.17 3.43 3.18 3.17 3.42 3.17 3.43 3.18 3.17 3.43 3.18 3.17 3.43 3.18 3.17 3.43 3.38 3.18 3.18 3.18 3.19 2.54 3.10 3.18 3.18 3.18 3.18 3.18 3.18 3.18 3.18		Z.48	2.52	0.87	1.55		2.10		3.13	1.30	1.82	4.89	28.73	18.97	12.40
2.40 2.21 4.13 3.41 1.63 2.01 4.20 4.64 4.83 4.11 36.31 17.20 1.47 4.46 5.12 6.25 2.11 2.41 2.18 2.27 3.68 3.57 36.79 22.78 1.91 2.78 3.86 4.26 3.77 4.48 3.87 5.37 3.79 5.16 43.24 18.20 5.44 1.54 3.38 2.22 4.17 3.70 3.63 1.35 3.22 2.69 39.50 29.46 1.54 3.38 2.22 4.17 3.70 3.63 1.35 3.22 2.69 39.50 2.946 4.00 3.05 3.99 3.66 3.16 2.81 4.11 1.51 5.27 3.13 39.81 2.3.7 2.78 1.93 1.34 2.85 7.35 4.45 6.71 3.29 3.92 4.461 21.51 3.22 2.69 5.82 7.73 2.66 3.88 4.28 6.06 1.30 2.24 4.71 4.24.06 4.45 2.83 1.26 1.65 2.67 7.72 5.47 4.50 5.59 5.65 45.75 20.84 1.35 2.16 1.11 2.66 1.14 2.94 5.32 2.86 1.64 3.60 30.85 25.32 0.97 3.28 3.75 1.11 0.91 5.85 5.15 3.13 4.92 1.77 35.84 17.35 2.16 1.11 2.64 1.14 2.94 5.32 2.84 1.15 3.10 3.08 3.08 3.08 3.08 3.08 3.08 3.08 3.0		3.75	0.32	2.94	2.88		3.79		2.88	3.98	4.52	1.35	33.27	14.96	16 47
1.47 4.46 5.12 6.25 2.11 2.41 2.18 2.27 3.68 3.57 36.79 22.78 1.91 2.78 3.86 4.26 3.77 4.48 3.87 5.37 3.79 5.16 43.24 18.20 3.75 3.70 4.11 5.4 15.4 3.8 2.22 4.17 3.70 3.63 1.35 3.22 2.69 3.950 2.946 3.75 5.61 4.38 2.44 1.54 3.8 4.26 1.69 3.71 3.08 3.56 5.13 41.30 2.440 4.00 3.05 3.99 3.44 3.46 1.69 3.71 3.08 3.56 5.13 41.30 2.440 4.00 3.05 3.99 3.44 3.46 1.69 3.71 3.08 3.56 5.13 41.30 2.440 4.00 3.05 3.99 3.42 8.67 3.5 4.75 6.71 3.29 3.92 3.68 4.461 2.151 3.22 2.69 5.82 7.73 2.66 3.88 4.28 6.06 1.30 2.24 4.714 2.406 4.45 2.83 1.26 1.65 2.67 7.72 5.47 4.50 5.59 5.65 45.75 20.84 4.5 1.11 2.66 1.14 2.94 5.32 2.86 1.64 3.60 3.0.85 2.53 3.35 3.38 3.75 1.11 0.91 5.85 5.15 3.13 4.92 1.77 35.84 17.35 2.16 1.11 2.66 1.14 2.94 5.32 2.86 1.64 3.60 3.0.85 2.53 3.33 5.38 0.89 4.01 6.42 2.16 3.78 4.87 3.49 2.66 3.928 2.0.82 1.30 2.84 4.20 4.11 2.61 3.92 1.11 2.65 1.14 5.24 2.14 4.52 5.26 2.74 4.11 2.61 3.92 1.73 3.18 2.18 1.81 3.21 4.89 4.57 5.13 4.74 1.15 2.61 3.88 1.29 1.85 5.27 3.48 1.92 1.61 8.82 2.34 3.10 2.84 4.20 4.178 19.85 2.57 2.48 4.80 3.23 2.89 1.81 3.21 4.89 5.47 3.22 3.38 3.16 3.03 3.91 8 23.13 1.29 3.04 2.95 1.73 3.88 2.96 3.74 2.95 3.75 1.80 3.91 8.25 3.75 1.80 3.91 8.25 3.75 1.80 3.91 8.80 3.29 3.70 3.91 8.80 3.70 3.91 8.80 3.70 3.91 8.80 3.70 3.91 8.80 3.70 3.91 8.70 3.70 3.70 3.70 3.70 3.70 3.70 3.70 3		1.08	2.40	2.21	4.13		1.63		4.20	4.64	4.83	4.1	36.31	17.20	15.38
1.91 2.78 3.86 4.26 3.77 4.48 3.87 5.37 3.79 5.16 43.24 18.20 5.44 1.54 3.38 2.22 4.17 3.70 3.63 1.35 3.22 2.69 39.50 29.46 3.75 2.30 4.61 6.82 6.07 2.52 1.90 2.55 4.25 4.75 45.92 19.71 2.26 5.61 4.38 3.44 3.46 1.69 3.71 3.08 3.56 5.13 41.30 2.44 4.00 3.05 3.99 3.66 3.15 2.81 4.11 1.51 5.27 3.71 39.81 23.37 2.72 2.69 1.34 2.85 7.35 4.45 6.71 3.29 3.65 5.13 41.30 2.44 4.61 2.72 2.63 1.34 2.85 7.35 4.45 6.71 3.29 3.65 1.34 2.85 7.35 2.66 3.88 4.28 6.06 1.30 2.24 47.14 24.06 4.45 2.83 1.26 1.85 2.67 7.72 5.47 4.50 5.59 5.65 45.75 20.84 1.35 2.16 1.11 2.66 1.85 2.67 7.72 5.47 4.50 5.59 5.65 39.28 20.82 1.35 2.16 1.11 2.66 1.81 2.85 2.15 1.19 0.91 5.85 5.15 3.13 4.92 1.77 35.84 17.35 2.83 3.58 0.89 4.01 6.42 2.16 3.78 4.87 3.49 2.66 39.28 20.82 1.30 2.87 3.16 2.12 4.89 4.57 5.13 4.71 2.14 1.75 37.26 19.81 2.65 2.21 2.14 5.24 2.14 4.52 5.26 2.74 4.11 2.61 39.27 19.11 1.85 5.27 3.48 1.92 1.61 8.82 2.34 3.10 3.88 9.29 44.32 19.33 1.62 4.20 4.64 2.27 2.42 4.32 2.59 1.00 2.91 4.52 36.38 27.98 2.75 1.50 1.30 1.82 4.80 3.23 2.82 5.14 3.50 3.83 3.16 3.03 3.18 2.3.13 1.50 3.04 2.96 1.74 2.73 4.47 5.35 3.48 6.26 1.60 40.11 20.43 2.14 4.85 5.44 2.75 3.48 4.20 4.13 3.13 3.13 3.13 3.13 3.13 3.13 3.13		0.79	1.47	4.46	5.12		2.11		2.18	2.27	3.68	3.57	36.79	22.78	18.07
5.44 1.54 3.38 2.22 4.17 3.70 3.63 1.35 3.22 2.69 39.50 29.46 3.75 2.30 4.61 6.82 6.07 2.52 1.90 2.55 4.25 4.75 45.92 19.71 2.26 5.61 4.38 3.44 3.46 1.69 3.71 3.08 3.56 5.13 41.30 2.4.40 4.00 3.05 3.99 3.66 3.15 2.81 4.11 1.51 5.27 3.71 39.81 23.37 2.78 1.93 1.34 2.85 7.35 4.45 6.71 3.29 3.92 3.68 44.61 21.51 3.27 2.78 1.93 1.34 2.85 7.73 2.66 3.88 4.28 6.06 1.30 2.24 47.14 2.406 4.45 2.83 1.26 1.65 2.67 7.72 5.47 4.50 5.59 5.65 45.75 20.84 1.35 2.16 1.11 0.91 2.65 3.13 4.92 1.64 3.60 30.85 25.32 0.97 3.28 3.75 1.11 0.91 4.29 5.35 2.86 1.64 3.60 30.85 25.32 0.97 3.28 3.75 1.11 0.91 4.29 5.15 3.13 4.92 1.65 39.28 20.82 1.30 2.87 3.16 2.12 4.89 4.57 5.13 4.71 2.14 1.75 37.26 19.81 2.65 2.21 2.14 5.24 2.14 4.52 5.26 2.74 4.11 2.61 39.27 19.11 1.85 5.27 3.48 1.92 1.61 8.82 2.34 3.10 3.88 9.29 44.32 19.33 1.62 4.20 4.64 2.27 2.42 4.32 2.59 1.00 2.91 4.52 36.38 27.98 2.31 1.85 5.27 3.48 1.92 1.61 8.82 2.34 3.10 3.88 9.29 44.32 19.85 2.57 2.46 2.48 4.50 2.31 2.64 4.74 3.65 5.84 4.20 4.178 19.85 2.57 2.46 2.48 4.50 2.31 2.64 4.74 3.65 5.84 4.20 4.178 19.85 2.31 1.50 3.04 2.96 1.74 2.73 4.31 5.33 3.48 6.26 1.60 40.11 2.043 2.14 4.85 5.14 3.54 3.54 3.51 3.43 3.53 3.18 2.51 2.44 3.54 3.57 3.43 3.54 3.57 3.43 3.53 3.54 3.57 3.54 3.55 3.54 3.57 3.54 3.55 3.54 3.57 3.54		2.50	1.91	2.78	3.86		3.77		3.87	5.37	3.79	5.16	43.24	18.20	20.24
3.75       2.30       4.61       6.82       6.07       2.52       1.90       2.55       4.75       45.92       19.71         2.26       5.61       4.38       3.44       3.46       1.69       3.71       3.08       3.56       5.13       41.30       24.40         4.00       3.05       3.99       3.66       3.15       2.81       4.11       1.51       5.27       3.71       39.81       23.37         2.78       1.93       1.34       2.85       7.35       4.45       6.71       3.29       3.92       3.68       44.61       21.51         3.22       2.69       5.82       7.73       2.66       3.88       4.28       6.06       1.30       2.24       47.14       24.06         4.45       2.83       1.26       3.88       4.28       6.06       1.30       2.24       47.14       24.06         4.45       2.83       1.26       3.44       4.50       5.25       5.65       45.75       5.084         1.35       2.16       1.11       2.06       3.84       4.80       5.47       4.50       5.59       5.65       45.75       5.08         4.45       2.86       1.11 <td></td> <td>4.64</td> <td>5.44</td> <td>.54</td> <td>3.38</td> <td></td> <td>4.17</td> <td></td> <td>3.63</td> <td>1.35</td> <td>3.22</td> <td>2.69</td> <td>39.50</td> <td>29.46</td> <td>17.10</td>		4.64	5.44	.54	3.38		4.17		3.63	1.35	3.22	2.69	39.50	29.46	17.10
2.26 5.61 4.38 3.44 3.46 1.69 3.71 3.08 3.56 5.13 41.30 24.40 4.00 3.05 3.99 3.66 3.15 2.81 4.11 1.51 5.27 3.71 39.81 23.37 2.78 1.93 1.34 2.85 7.35 4.45 6.71 3.29 3.92 3.68 44.61 21.51 3.22 2.69 5.82 7.73 2.66 3.88 4.28 6.06 1.30 2.24 47.14 24.06 4.45 2.83 1.26 1.65 2.67 7.72 5.47 4.50 5.59 5.65 45.75 20.84 1.35 2.16 1.11 2.66 1.14 2.94 5.32 2.86 1.64 3.60 30.85 25.32 0.97 3.28 3.75 1.11 0.91 5.85 5.15 3.13 4.92 1.77 35.84 17.35 3.33 5.38 0.89 4.01 6.42 2.16 3.78 4.87 3.49 2.66 39.28 20.82 1.30 2.87 3.16 2.12 4.89 4.57 5.13 4.71 2.14 1.75 37.26 19.81 2.65 2.21 2.14 5.24 2.14 4.52 5.26 2.74 4.11 2.61 39.27 19.11 1.85 5.27 3.48 1.92 1.61 8.82 2.34 3.10 3.88 9.29 44.32 19.33 1.62 4.20 4.64 2.27 2.42 4.32 2.59 1.00 2.91 4.52 36.38 27.98 2.57 2.46 2.48 4.50 2.31 2.64 4.74 3.65 5.84 4.20 41.78 19.85 2.88 1.81 3.21 4.89 5.47 3.22 3.38 3.36 3.39 3.18 23.13 1.50 1.97 1.82 4.80 3.23 2.82 5.14 3.50 3.79 2.58 35.72 17.61 2.40 3.04 2.96 1.74 2.73 4.31 2.46 5.65 4.46 1.57 3.43 3.8.36 20.58 2.40 3.04 3.17 3.42 3.19 4.06 3.74 3.3 3.43 3.8.36 20.58		4.70	3.75	2.30	4.61	6.82	6.07	2.52	1.90	2.55	4.25	4.75	45.92	19.71	21.92
4.00 3.05 3.99 3.66 3.15 2.81 4.11 1.51 5.27 3.71 39.81 23.37 2.78 1.93 1.34 2.85 7.35 4.45 6.71 3.29 3.92 3.68 44.61 21.51 3.22 2.69 5.82 7.73 2.66 3.88 4.28 6.06 1.30 2.24 47.14 24.06 4.45 2.83 1.26 1.65 2.67 7.72 5.47 4.50 5.59 5.65 45.75 20.84 1.35 2.16 1.11 2.66 1.14 2.94 5.32 2.86 1.64 3.60 30.85 25.32 0.97 3.28 3.75 1.11 0.91 5.85 5.15 3.13 4.92 1.77 35.84 17.35 3.33 5.38 0.89 4.01 6.42 2.16 3.78 4.87 3.49 2.66 39.28 20.82 1.30 2.87 3.16 2.12 4.89 4.57 5.13 4.71 2.14 1.75 37.26 19.81 2.65 2.21 2.14 5.24 2.14 4.52 5.26 2.74 4.11 2.61 39.27 19.11 1.85 5.27 3.48 1.92 1.61 8.82 2.34 3.10 3.88 9.29 44.32 19.33 1.62 4.20 4.64 2.27 2.42 4.32 2.59 1.00 2.91 4.52 36.38 27.98 2.57 2.46 2.48 4.50 2.31 2.64 4.74 3.65 5.84 4.20 41.78 19.85 2.57 2.46 2.48 4.50 2.31 2.46 5.65 4.46 1.57 3.41 1.20 3.04 2.96 1.74 2.73 4.31 2.46 5.65 4.46 1.57 3.47 1.87 3.51 4.86 5.19 2.65 4.47 5.33 3.48 6.26 1.60 40.11 20.43 2.11 4.86 5.19 5.04 3.87 3.74 3.34 3.36 3.38 20.58 10.81 3.17 3.42 3.19 4.06 3.74 3.34 3.76 3.43 3.8.36 20.58		47.7	2.26	5.61	4.38	3.44	3.46	1.69	3.71	3.08	3.56	5.13	41.30	24.40	16.68
2.78 1.93 1.34 2.85 7.35 4.45 6.71 3.29 3.92 3.68 44.61 21.51 3.22 2.69 5.82 7.73 2.66 3.88 4.28 6.06 1.30 2.24 47.14 24.06 4.45 2.83 1.26 1.65 2.67 7.72 5.47 4.50 5.59 5.65 45.75 20.84 1.35 2.16 1.11 2.66 1.14 2.94 5.32 2.86 1.64 3.60 30.85 25.32 0.97 3.28 3.75 1.11 0.91 5.85 5.15 3.13 4.92 1.77 35.84 17.35 3.33 5.38 0.89 4.01 6.42 2.16 3.78 4.87 3.49 2.66 39.28 20.82 1.30 2.87 3.16 2.12 4.89 4.57 5.13 4.71 2.14 1.75 37.26 19.81 2.65 2.21 2.14 5.24 2.14 4.52 5.26 2.74 4.11 2.61 39.27 19.11 1.85 5.27 3.48 1.92 1.61 8.82 2.34 3.10 3.88 9.29 44.32 19.33 1.62 4.20 4.64 2.27 2.42 4.32 2.59 1.00 2.91 4.52 36.38 27.98 2.57 2.46 2.48 4.50 2.31 2.64 4.74 3.65 5.84 4.20 41.78 19.85 2.58 1.81 3.21 4.89 5.47 3.22 3.38 3.38 3.16 3.03 3.918 2.3.13 1.50 1.97 1.82 4.80 3.23 2.82 5.14 3.50 3.79 2.58 35.72 1.761 1.29 3.04 2.96 1.74 2.73 4.31 2.46 5.65 4.46 1.57 34.71 1.8.70 3.51 2.41 4.86 5.19 5.04 3.89 2.42 2.73 6.44 2.45 4.50 4.638 2.5.66 2.40 3.04 3.17 3.43 3.76 3.43 3.83 2.95 8.05 2.40 3.04 3.17 3.43 3.76 3.43 3.83 2.95 8.05 2.40 3.04 3.17 3.43 3.76 3.43 3.83 2.95 8.05 2.40 3.04 3.17 3.42 3.19 4.06 3.74 3.76 3.43 3.83 3.83 3.83 3.83 3.83 3.83 3.83		- 65 - 1	4.00	3.05	3.99	3.66	3.15	2.81	4.1	1.51	5.27	3.71	39.81	23.37	17.72
3.22       2.69       5.82       7.73       2.66       3.88       4.28       6.06       1.30       2.24       47.14       24.06         4.45       2.83       1.26       1.65       2.67       7.72       5.47       4.50       5.59       5.65       45.75       20.84         1.35       2.16       1.11       2.66       1.14       2.94       5.32       2.86       1.64       3.60       30.85       25.32         0.97       3.28       3.75       1.11       0.91       5.85       5.15       3.13       4.92       1.77       35.84       17.35         3.33       5.38       0.89       4.01       6.42       2.16       3.78       4.87       3.49       2.66       39.28       20.82         1.30       2.87       3.16       2.12       4.89       4.57       5.13       4.71       2.14       1.75       37.26       19.81         2.65       2.21       2.14       4.52       5.26       2.74       4.11       2.41       35.27       19.11         1.62       4.20       4.64       2.27       2.42       4.32       2.59       1.00       2.91       4.52       3.63       3.78 <td></td> <td>70.0</td> <td>Z. / Ø</td> <td>1.93</td> <td>1.34</td> <td>2.85</td> <td>7.35</td> <td>4.45</td> <td>6.71</td> <td>3.29</td> <td>3.92</td> <td>3.68</td> <td>44.61</td> <td>21.51</td> <td>22.70</td>		70.0	Z. / Ø	1.93	1.34	2.85	7.35	4.45	6.71	3.29	3.92	3.68	44.61	21.51	22.70
4.45       2.83       1.26       1.65       2.67       7.72       5.47       4.50       5.59       5.65       45.75       20.84         1.35       2.16       1.11       2.66       1.14       2.94       5.32       2.86       1.64       3.60       30.85       25.32         0.97       3.28       3.75       1.11       0.91       5.85       5.15       3.13       4.92       1.77       35.84       17.35         3.33       5.38       0.89       4.01       6.42       2.16       3.78       4.87       3.49       2.66       39.28       20.82         1.30       2.87       3.16       2.12       4.89       4.57       5.13       4.71       2.14       1.75       37.26       19.81         2.65       2.21       2.14       4.52       5.13       4.71       2.14       1.75       37.26       19.81         2.65       2.27       3.48       1.92       1.61       8.82       2.34       3.10       3.88       9.29       4.32       19.11         1.62       4.20       4.64       2.27       2.42       4.32       2.59       1.00       2.91       4.52       3.63       2.34			5.22	2.69	5.82	7.73	2.66	3.88	4.28	90.9	1.30	2.24	47.14	24.06	24.37
1.35 2.16 1.11 2.66 1.14 2.94 5.32 2.86 1.64 3.60 30.85 25.32 0.97 3.28 3.75 1.11 0.91 5.85 5.15 3.13 4.92 1.77 35.84 17.35 3.33 5.38 0.89 4.01 6.42 2.16 3.78 4.87 3.49 2.66 39.28 20.82 1.30 2.87 3.16 2.12 4.89 4.57 5.13 4.71 2.14 1.75 37.26 19.81 2.65 2.21 2.14 5.24 2.14 4.52 5.26 2.74 4.11 2.61 39.27 19.11 1.85 5.27 3.48 1.92 1.61 8.82 2.34 3.10 3.88 9.29 44.32 19.33 1.62 4.20 4.64 2.27 2.42 4.32 2.59 1.00 2.91 4.52 36.38 2.798 2.57 2.46 2.48 4.50 2.31 2.64 4.74 3.65 5.84 4.20 41.78 19.85 2.57 2.46 2.48 4.50 2.31 2.64 4.74 3.65 5.84 4.20 41.78 19.85 2.57 2.46 2.48 8.52 3.31 2.64 4.74 3.65 5.84 6.20 41.78 19.85 1.50 1.97 1.82 4.80 3.23 2.82 5.14 3.50 3.79 2.58 35.72 17.61 1.29 3.04 2.96 1.74 2.73 4.31 2.46 5.65 4.46 1.57 3.471 1.870 3.51 2.21 4.38 3.19 2.65 4.47 5.33 3.48 6.26 1.60 40.11 20.43 2.11 4.86 5.19 5.04 3.89 2.42 2.73 6.44 2.45 4.50 46.38 25.06 2.40 3.04 3.17 3.42 3.19 4.06 3.74 3.34 3.76 3.43 38.38 20.58		. S. C	4.43 7.43	2.83	1.26	1.65	2.67	7.72	5.47	4.50	5.59	5.65	45.75	20.84	18.77
0.97       5.28       3.75       1.11       0.91       5.85       5.15       3.13       4.92       1.77       35.84       17.35         3.33       5.38       0.89       4.01       6.42       2.16       3.78       4.87       3.49       2.66       39.28       20.82         1.30       2.87       3.16       2.12       4.89       4.57       5.13       4.71       2.14       1.75       37.26       19.81         2.65       2.21       2.14       5.24       2.14       4.52       5.26       2.74       4.11       2.61       39.27       19.11         1.85       5.27       3.48       1.92       1.61       8.82       2.34       3.10       3.88       9.29       44.32       19.11         1.62       4.20       4.64       2.27       2.42       4.32       2.59       1.00       2.91       4.52       36.38       27.38       36.38       27.38       36.38       27.38       36.38       27.38       36.38       27.38       37.83       37.83       36.38       37.83       37.83       37.83       36.38       37.83       37.83       37.83       37.83       37.83       37.83       37.83       37.83<		0.65		2.16	<del>-</del>	2.66	<u></u>	2.94	5.32	2.86	1.64	3.60	30.85	25.32	13.17
3.55 5.58 0.89 4.01 6.42 2.16 3.78 4.87 3.49 2.66 39.28 20.82 1.30 2.87 3.16 2.12 4.89 4.57 5.13 4.71 2.14 1.75 37.26 19.81 2.65 2.21 2.14 5.24 2.14 4.52 5.26 2.74 4.11 2.61 39.27 19.11 1.85 5.27 3.48 1.92 1.61 8.82 2.34 3.10 3.88 9.29 44.32 19.33 1.62 4.20 4.64 2.27 2.42 4.32 2.59 1.00 2.91 4.52 36.38 2.798 2.57 2.46 2.48 4.50 2.31 2.64 4.74 3.65 5.84 4.20 41.78 19.85 2.88 1.81 3.21 4.89 5.47 3.22 3.38 3.16 3.03 39.18 23.13 1.50 1.97 1.82 4.80 3.23 2.82 5.14 3.50 3.79 2.58 35.72 17.61 1.29 3.04 2.96 1.74 2.73 4.31 2.46 5.65 4.46 1.57 34.71 18.70 3.51 2.21 4.38 3.19 2.65 4.47 5.33 3.48 6.26 1.60 40.11 20.43 2.11 4.86 5.19 5.04 3.89 2.42 2.73 6.44 2.45 4.50 46.38 25.06 2.40 3.04 3.17 3.42 3.19 4.06 3.74 3.34 3.76 3.43 38.38 20.58		<del>-</del> 6	1.97	3.28	5.75	<del>-</del>	0.91	5.85	5.15	3.13	4.92	1.77	35.84	17.35	16.77
1.50 2.87 3.16 2.12 4.89 4.57 5.13 4.71 2.14 1.75 37.26 19.81 2.65 2.21 2.14 5.24 2.14 4.52 5.26 2.74 4.11 2.61 39.27 19.11 1.85 5.27 3.48 1.92 1.61 8.82 2.34 3.10 3.88 9.29 44.32 19.33 1.62 4.20 4.64 2.27 2.42 4.32 2.59 1.00 2.91 4.52 36.38 2.798 2.57 2.46 2.48 4.50 2.31 2.64 4.74 3.65 5.84 4.20 41.78 19.85 2.88 1.81 3.21 4.89 5.47 3.22 3.38 3.38 3.16 3.03 39.18 23.13 1.50 1.97 1.82 4.80 3.23 2.82 5.14 3.50 3.79 2.58 35.72 17.61 1.29 3.04 2.96 1.74 2.73 4.31 2.46 5.65 4.46 1.57 34.71 18.70 3.51 2.21 4.38 3.19 2.65 4.47 5.33 3.48 6.26 1.60 40.11 20.43 2.11 4.86 5.19 5.04 3.89 2.42 2.73 6.44 2.45 4.50 4.53 25.06 2.40 3.04 3.17 3.42 3.19 4.06 3.74 3.34 3.76 3.43 38.38 20.58		0.04 0.04	5.55	5.58	0.89	4.01	42	2.16	3.78	4.87	3.49	2.66	39.28	20.82	17.26
2.65 2.21 2.14 5.24 2.14 452 5.26 2.74 4.11 2.61 39.27 19.11 1.85 5.27 3.48 1.92 1.61 8.82 2.34 3.10 3.88 9.29 44.32 19.33 1.62 4.20 4.64 2.27 2.42 4.32 2.59 1.00 2.91 4.52 36.38 27.98 2.57 2.46 2.48 4.50 2.31 2.64 4.74 3.65 5.84 4.20 41.78 19.85 2.88 1.81 3.21 4.89 5.47 3.22 3.38 3.36 3.16 3.03 39.18 23.13 1.50 1.97 1.82 4.80 3.23 2.82 5.14 3.50 3.79 2.58 35.72 17.61 1.29 3.04 2.96 1.74 2.73 4.31 2.46 5.65 4.46 1.57 3.471 18.70 3.51 2.21 4.38 3.19 2.65 4.47 5.33 3.48 6.26 1.60 40.11 20.43 2.11 4.86 5.19 5.04 3.89 2.42 2.73 6.44 2.45 4.50 4.53 25.06 2.40 3.04 3.17 3.42 3.19 4.06 3.74 3.34 3.76 3.43 30.36 20.58 10.88 11/83 4/85		0.0 0.0	05.0	7.87	3.16	2.12	89	4.57	5.13	471	2.14	1.75	37.26	19.81	19.87
1.85 5.27 5.48 1.92 1.61 8.82 2.34 3.10 3.88 9.29 44.32 19.33 1.62 4.20 4.64 2.27 2.42 4.32 2.59 1.00 2.91 4.52 36.38 27.98 2.57 2.46 2.48 4.50 2.31 2.64 4.74 3.65 5.84 4.20 41.78 19.85 2.88 1.81 3.21 4.89 5.47 3.22 3.38 3.38 3.16 3.03 39.18 23.13 1.50 1.97 1.82 4.80 3.23 2.82 5.14 3.50 3.79 2.58 35.72 17.61 1.29 3.04 2.96 1.74 2.73 4.31 2.46 5.65 4.46 1.57 3.471 18.70 3.51 2.21 4.38 3.19 2.65 4.47 5.33 3.48 6.26 1.60 40.11 20.43 2.11 4.86 5.19 5.04 3.89 2.42 2.73 6.44 2.45 4.50 4.538 25.06 2.40 3.04 3.17 3.42 3.19 4.06 3.74 3.34 3.76 3.43 30.38 20.58		77.7	2.65	2.21	2.14	5.24	4	4.52	5.26	2.74	4.11	2.61	39.27	19.11	19.30
1.62 4.20 4.64 2.27 2.42 4.32 2.59 1.00 2.91 4.52 36.38 27.98 2.57 2.46 2.48 4.50 2.31 2.64 4.74 3.65 5.84 4.20 41.78 19.85 2.88 1.81 3.21 4.89 5.47 3.22 3.38 3.38 3.16 3.03 39.18 23.13 1.50 1.97 1.82 4.80 3.23 2.82 5.14 3.50 3.79 2.58 35.72 17.61 1.29 3.04 2.96 1.74 2.73 4.31 2.46 5.65 4.46 1.57 34.71 18.70 3.51 2.21 4.38 3.19 2.65 4.47 5.33 3.48 6.26 1.60 40.11 20.43 2.11 4.86 5.19 5.04 3.89 2.42 2.73 6.44 2.45 4.50 46.38 25.06 2.40 3.04 3.17 3.42 3.19 4.06 3.74 3.34 3.76 3.43 30.38 20.58		- 1	. g	5.27	₹.	1.92	<u>-</u>	8.82	2.34	3.10	3.88	9.29	44.32	19.33	18.17
2.57       2.46       2.48       4.50       2.31       2.64       4.74       3.65       5.84       4.20       41.78       19.85         2.88       1.81       3.21       4.89       5.47       3.22       3.38       3.36       3.16       3.03       39.18       23.13         1.50       1.97       1.82       4.80       3.23       2.82       5.14       3.50       3.79       2.58       35.72       17.61         1.29       3.04       2.96       1.74       2.73       4.31       2.46       5.65       4.46       1.57       34.71       18.70         3.51       2.21       4.38       3.19       2.65       4.47       5.33       3.48       6.26       1.60       40.11       20.43         2.11       4.86       5.19       5.04       3.89       2.42       2.73       6.44       2.45       4.50       46.38       25.06         2.40       3.04       3.93       4.06       3.74       3.34       3.76       3.43       30.38       20.58         10/83       11/83       4/85		C7.7	70.	4.20	4.64	2.27	42	4.32	2.59	1.00	2.91	4.52	36.38	27.98	16.24
2.88       1.81       3.21       4.89       5.47       3.22       3.38       3.36       3.16       3.03       39.18       23.13         1.50       1.97       1.82       4.80       3.23       2.82       5.14       3.50       3.79       2.58       35.72       17.61         1.29       3.04       2.96       1.74       2.73       4.31       2.46       5.65       4.46       1.57       34.71       18.70         3.51       2.21       4.38       3.19       2.65       4.47       5.33       3.48       6.26       1.60       40.11       20.43         2.11       4.86       5.19       5.04       3.89       2.42       2.73       6.44       2.45       4.50       46.38       25.06         2.40       3.04       3.17       3.42       3.13       3.43       30.38       20.58         10/83       11/83       4/85		0.00 100 100	7.57	2.46	2.48	4.50	31	2.64	4.74	3.65	5.84	4.20	41.78	19.85	16.67
1.50 1.97 1.82 4.80 3.23 2.82 5.14 3.50 3.79 2.58 35.72 17.61 1.29 3.04 2.96 1.74 2.73 4.31 2.46 5.65 4.46 1.57 34.71 18.70 3.51 2.21 4.38 3.19 2.65 4.47 5.33 3.48 6.26 1.60 40.11 20.43 2.11 4.86 5.19 5.04 3.89 2.42 2.73 6.44 2.45 4.50 46.38 25.06 2.40 3.04 3.17 3.42 3.19 4.06 3.74 3.34 3.76 3.43 38.38 20.58 10/83 11/83 4/85		S : 5	2.88	1.81	3.21	4.89	47	3.22	3.38	3.38	3.16	3.03	39.18	23.13	20.17
1.29 3.04 2.96 1.74 2.73 4.31 2.46 5.65 4.46 1.57 34.71 18.70 3.51 2.21 4.38 3.19 2.65 4.47 5.33 3.48 6.26 1.60 40.11 20.43 2.11 4.86 5.19 5.04 3.89 2.42 2.73 6.44 2.45 4.50 46.38 25.06 2.40 3.04 3.17 3.42 3.19 4.06 3.74 3.34 3.76 3.43 38.38 20.58 10/83 11/83 4/85		0.54 1.154	1.50	1.97	1.82	4.80	.23	2.82	5.14	3.50	3.79	2.58	35.72	17.61	17.81
3.51 2.21 4.38 3.19 2.65 4.47 5.33 3.48 6.26 1.60 40.11 20.43 2.11 4.86 5.19 5.04 3.89 2.42 2.73 6.44 2.45 4.50 46.38 25.06 2.40 3.04 3.17 3.42 3.19 4.06 3.74 3.34 3.76 3.43 38.38 20.58 10/83 11/83 4/85		5.57	1.29	3.04	2.96	1.74	.73	4.31	2.46	5.65	4.46	1.57	34.71	18.70	14.20
2.11 4.86 5.19 5.04 3.89 2.42 2.73 6.44 2.45 4.50 46.38 25.06 19 2.40 3.04 3.17 3.42 3.19 4.06 3.74 3.34 3.76 3.43 30.36 20.56 17.10/83 11/83 4/85		1.33	3.51	2.21	4.38	3.19	99	4.47	5.33	3.48	6.26	1.60	40.11	20.43	20.02
2.40 3.04 3.17 3.42 3.19 4.06 3.74 3.34 3.76 3.43 38.38 20.58 17.10/83 11/83 4/85		3.38	2.11	4.86	5.19	5.04	89	2.42	2.73	6.44	2.45	4.50		25.06	19.27
3 10/83 11/83 4/85		2.20		3.04	3,17	3.42	3.19	4.06	3.74	3,34	3.76	3.43			
			`	11/83	4/85					· ·	  -  -	!	) ) !		
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US SNOW SURVEY DATA, LAKE ONTARIO BASIN

	A	В	С		Ε	F	6	1 0
	<del>                                     </del>			<del>                                     </del>	<u> </u>			H H
2	DATA	FOR BASIN	<u></u>	CT.TE OF	151.1.110.011		ATTACHM	CHIA-3
$\frac{2}{3}$		· · · · · · · · · · · · · · · · · · ·		STATE OF				
4	Station	Date	Period =		Water Equiv			ļ
5	COI C	ANADICE AND	HEM! OCK I	INCHES	INCHES I/	2/	<del> </del>	
6	CO1	600104	I I	2.7	0.6	A		ļ
1 5	COI	600201	2	43	1.17	Â	<del></del>	
8	CO1	600301	3	16.7	3.81	A	<del></del>	<del> </del>
9	C01	600314	4	169	4 48	Ä		
10	C01	610103	1	14.2	2.03	Â	<del>                                     </del>	<u> </u>
1 1	CO1	610131	2	10.1	2.46	A	· · · · · · · · · · · · · · · · · · ·	
12	CO1	610227	3	3	0.9	A		
13	CO1	610313	4	3.9	0.91	Α		
	<u>CO1</u>	620109		0.4	0 1	A_		
15	CO1	620205	2	0.2	0.03	Α		
16	CO1	620505	3	5 2	185	Α		<u> </u>
17	CO1	620319	4	2 3	0.74	A		
1.8	COI	630107	1	7.6	184	A		
	CO1	630205 630304	2	117	3 23			
	CO1	630304 630318	3 4	13.2 5.9	4.42	A	-	ļ
	COI	640107	1	9.1	1.87 2.09	Α	ļ. <del>-</del>	
	COI	640203	2	3.2	0.81	A	<del> </del>	
	ÇO I	640316	4	1.5	0.73	Â	<del> </del>	<del></del>
	C01	650104	1	5 1	1.06	Ā		
	C01	650201	2	8.9	1.45	A		
	CO1	650302	3	1.6	0.37	A		
	C01	650315	4	4.3	0.44	Α		
	CO1	660103	1	0	0	A		
	COI	660121	2	19.2	4.21	A		
	CO1	670109	1 1	1.8	0.46	Α		
	C01	670130	2	6.8	0.89	Α		<u> </u>
	CO1	670227	3	3.9	0.89	Α		
34	CO1	670313	4	0.8	0.22	<u> </u>		
	COI	680304 680318	3	4.6	0.69	A		
	COI	690107	4	0.9	0.3	A		
	COI	690204	2	2 7	0.54	A		<del></del>
39		690304	3	5.3	1.31	- A		,
	COI	690317	4	5.5	1.62	A		
	coi	690331	5	0.4	0.05	<del></del>		
	COI	700205	2	10.3	211	Ā		
	coi	700304	3	8 3	2.82	Ā	· ·	
	COI	700319	4	7.5	1.67	Ä		
45	COI	700401	5	14.1	0.85	A		
46		710201	2	7.6	2.28	A		
	COI	710304	3	6 2	3 19	Α		
48		710315	4	6.4	2 5 7	A		
49		710329	5	2.7	0 9 7	Α		
50		710413	6	0	0	Α		
	COI	720103	1	3.7	0.88	A		
52	201	720201	2	3.3	0 44	A		
	201	720228	3	15.2	3.68	Α		
54		720314	4	5.8	2.02	A		
	201	720327	5	2.4	0.68	<u>A</u>		
56 0	201	730102	1	0	0 75	<u> </u>		
58		730130 730226	2 3	3.9	0.35	<u> </u>		
59	01	730226	4	7.4	2 08	<u> </u>		
60	01	730312	5	0 1	0	- <u>A</u>		
61		740109	1	1.8	0.25	<del>^</del>		
62		740204	2	4.4	0.23	Â		
63		740305	3	0	0 30	<del>- 2</del> -	-	
64 0		740320	4	2.6	0.63	Â		
65 0		740403	5	0	0.03	Â		
66		750108	ī	8.7	19			
67 0		750204	2	3.6	054			
68 (		750304	3	3.2	0.79			
69 0	·	750319	4	0	0			[
		<u></u>		L	<u> </u>	<u>!</u>		<del></del>

US SNOW SURVEY DATA, LAKE ONTARIO BASIN

38 38 38 38 38 38 38 39 CAN 39 39 39 39 39 39 49 49 49 49 49 49 49 49 49 4	880104 880201 880229 880314 880328 890130 390227 390313	C 1 2 3 4 5 6 1 2 3 4 5 5 6 1 2 3 4 5 5 5 2	D 8.2 9 10.7 10.8 10.4 1.7 15 16.8 14.1 6.6 0.5 0	E 1 2 2.7 3.4 3.8 99 2.2 3.6 4.1 2.8 0.14 0	F		G	H
338 338 338 338 338 338 338 338	890131 890227 890314 890328 890410 900102 900226 900314 900328 900410 00N 880104 880201 880229 880314 880328 890130 390227 390313	2 3 4 5 6 1 2 3 4 5 6	9 10.7 10.8 10.4 1.7 15 16.8 14.1 6.6 0.5 0	1 2 2,7 3,4 3,8 -99 2,2 3,6 4,1 2,8 0,14 0				H
338 338 338 338 338 338 338 338	890227 890314 890328 890410 900102 900131 900226 900314 900328 900410 00N 880104 880201 880229 880314 880328 890130 390227 390313	3 4 5 6 1 2 3 4 5 6	9 10.7 10.8 10.4 1.7 15 16.8 14.1 6.6 0.5 0	2 2.7 3.4 3.8 99 2.2 3.6 4.1 2.8 0.14 0				
38 38 38 38 38 38 38 38 38 38	890227 890314 890328 890410 900102 900131 900226 900314 900328 900410 00N 880104 880201 880229 880314 880328 890130 390227 390313	3 4 5 6 1 2 3 4 5 6	10.7 10.8 10.4 1.7 15 16.8 14.1 6.6 0.5 0	2.7 3.4 3.8 99 2.2 3.6 4.1 2.8 0.14 0				
38 38 38 38 38 38 38 38 38 39 CANT 39 39 69 69 69 69 69 69 69 69 69 6	890314 890328 890410 900102 900131 900226 900314 900328 900410 (ON 880104 880201 880229 880314 980328 390130 390227	4 5 6 1 2 3 4 5 6	10.8 10.4 1.7 15 16.8 14.1 6.6 0.5 0	3.4 3.8 99 2.2 3.6 4.1 2.8 0.14 0				
38 38 38 38 38 38 38 38 38 39 CANT 39 39 69 69 69 69 69 69 69 69 69 6	890328 890410 900102 900131 900226 900314 900328 900410 ON 880104 880201 880229 880314 880328 390130 390227 390313	5 6 1 2 3 4 5 6	10.4 1.7 1.5 1.6.8 1.4.1 6.6 0.5 0	3.8 99 2.2 3.6 4.1 2.8 0.14 0				
38 38 38 38 38 38 38 38 39 CAN 39 39 69 69 89 89 89 89 89	890410 900102 900131 900226 900314 900328 900410 ON 880104 880201 880229 880314 880328 390130 390227 390313	6 1 2 3 4 5 6	1.7 15 16.8 14.1 6.6 0.5 0	-99 22 36 41 28 014 0				
38 38 38 38 38 38 38 39 29 20 39 20 39 39 39 39 39 20 40 40 40 40 40 40 40 40 40 40 40 40 40	900102 900131 900226 900314 900328 900410 00N 880104 880201 880229 880314 880328 390130 390227 390313	1 2 3 4 5 6 5 5 2	15 16.8 14.1 6.6 0.5 0	-99 22 36 41 28 014 0				
38 38 38 38 38 39 39 39 39 39 39 39 39 39 39	900131 900226 900314 900328 900410 FON 880104 880201 880229 880314 880328 890130 890227 890313	2 3 4 5 6	15 16.8 14.1 6.6 0.5 0	2 2 3 6 4 1 2 8 0 1 4 0				
38   38   38   38   39   39   39   39	900131 900226 900314 900328 900410 FON 880104 880201 880229 880314 880328 890130 890227 890313	2 3 4 5 6	16.8 14.1 6.6 0.5 0	3 6 4 1 2 8 0 1 4 0				
38   38   38   38   39   39   39   39	900226 900314 900328 900410 ON 880104 880201 880229 880324 880328 390130 390227 390313	3 4 5 6 	14.1 6.6 0.5 0	4 1 2 8 0 14 0				
38 38 38 39 39 39 39 39 39 39 49 49 49 49 49 49 49 49 49 4	900314 900328 900410 FON 880104 880201 880229 880314 880328 890130 390227 390313	4   5   6     1   2   3   4   5   5   2	6.6 0.5 0	2 8 0 1 4 0				
38 38 39 CANT 39 39 39 39 39 49 49 49 49 49 49 49 49 49 4	900328 900410 FON 880104 880201 880229 880314 880328 890130 390227 390313 390327	5 6 1 2 3 4 5 2	0.5	2 8 0 1 4 0				
38 39 CANT 39 39 39 39 39 49 49 49 89 89 89 89 89	900410 600 880104 880201 880229 880314 880328 890130 390227 390313	6 2 3 4 5	0.5	0.14				
38   39   CAN   39   39   39   39   39   39   39   3	900410 600 880104 880201 880229 880314 880328 890130 390227 390313	6 2 3 4 5	1 0 0	- 1 0				
39 CAN 39 39 39 39 39 39 39 39 39 39 39 39 39 3	880104 880201 880229 880314 880328 890130 390227 390313	1 2 3 4 5	0 0	-1				
39 39 39 39 39 39 49 49 49 49 49 49 49 49 49 49 49 49 49	880104 880201 880229 880314 880328 890130 390227 390313	2 3 4 5	0	0.				
39 39 39 39 39 49 49 49 49 49 49 49 49 49 49 49 49 49	880201 880229 880314 880328 390130 390227 390313	2 3 4 5	0	0.		<del> </del>	<u>-</u>	
39 39 39 39 39 39 49 89 9 9 9	880229 880314 880328 890130 890227 390313	3 4 5 2	0	0.		7		
39 39 39 39 39 39 49 89 9 9 9	880229 880314 880328 890130 890227 390313	3 4 5 2	0			<del></del>		
39 39 39 39 39 49 89 9 89 9 9	880314 880328 890130 890227 390313	5 2	<del></del>					
39 39 49 49 49 49 49 49 49 49 49 49 49 49 49	380328 390130 390227 390313	5 2	0	-1		<del></del>	<del></del>	
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9 8 9 8 9 8 9 8 9 8	390130 390227 390313 390327	2			<del></del>			
9 8 9 8 9 8 9 9 9 9	390227 390313 390327	<del>2</del>	0	0	_{{1}}	1		
9 8 9 8 9 9 9 9	390313 390327	1	0	+ 1			<del></del>	
9 8 9 8 9 9	390327	3	0	-1		+		
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9 6	130321			-99	1	L		
9 9		5	0	-1				
9 9	390410	6	0	- 1	<del> </del>	<del> </del> -	<del></del>	
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#### SNOW SURVEY STATIONS IN US, LAKE ONTARIO BASIN

						ATTACHMENT A-4
	Station No	CANADICE AND HEMLOCK LAKES, N.Y. CHURCHVILLE, N.Y. GARBUTT, N.Y. MT. MORRIS, N.Y. RAYMOND, PA. ROCHESTER (AIRPORT), N.Y. SCIO (WELLSVILLE), N.Y. WARSAW, N.Y. WHITESVILLE, N.Y. ANGELICA, N.Y. AVON, N.Y. DANSVILLE, N.Y. HEMLOCK, N.Y. PAVILLION, N.Y. PORTAGEVILLE, N.Y. HEMLOCK, N.Y. BERGEN, N.Y. CANASERAGA, N.Y DANSVILLE, N.Y. HONEOYE, N.Y. WISCOY, N.Y. MT. MORRIS DAM, N.Y RUSHFORD LAKE, N.Y. WYOMING, N.Y. BALDWINSVILLE (LOCK 24), N.Y. DRESSERVILLE, N.Y. INW CAYUGA (LOCK 1), N.Y. CLYDE (LOCK 26), N.Y. DRYDEN, N.Y. ITALY, N.Y. NORTH LANSING, N.Y. MACEDOUGALL, N.Y. MACEDOUGALL, N.Y. MACEDOUGALL, N.Y. MACEDOUGALL, N.Y. MACEDON (LOCK 30), N.Y. MACEDOUGALL, N.Y. MACEDOUGA	Latitude	Longitude	Elevation	ATTACICIENT A-4
C	1 *	CANADICE AND HEMLOCK LAKES, N.Y.	42.72	77.58		
C C	2 * 3 *	CHURCHVILLE, N.Y.	43.10	77.88		
Ċ	4 *	MT. MORRIS. N.Y	43.02	77.78 77.90		
С	5 *	RAYMOND, PA	41.87	77.87		
С	6 *	ROCHESTER (AIRPORT), N.Y.	43.12	77.67		
C	7 <del>*</del>	SCIO (WELLSVILLE), N.Y.	42.17	77.98		
C C	8 * 9 *	WARSAW, N.Y.	42.68	78.20		
Ċ	10	ANGELICA NY	42.17 42.30	77.77 78.02		
č	} [	AVON, N.Y.	42.30	77.75		
С	12	DANSVILLE, N.Y.	42.57	77.70		
C	14	HEMLOCK, N.Y.	42.78	77.62	902	
C C	16	PAVILLION, N.Y.	42.88	78.03		
C	17 18	PURTAGEVILLE, N.Y.	42.57	78.05		
C	19	WISCOY, N.Y.	42.40	78.27 78.07		
C	60	BERGEN, N.Y.	43 10	77.93	574	
C	61	CANASERAGA, N.Y	42.47	77.77	1270	
C	62	DANSVILLE, N.Y.	42.55	77.72		
	63	HONEOYE, N.Y.	42.83	77.53		
C C	64 65	PUSHEODO LAKE NY	42.72	77.90 78.23	910	
Ċ	66	WELLSVILLE NY	42.30	77.93	1455 1505	
С	67	WYOMING, N.Y.	42.82	78.10	975	
D	*	BALDWINSVILLE (LOCK 24), N.Y.	43.15	76.33	3/9	
D	2	DRESSERVILLE, NY. INW	42 72	76.35	1160	
D	3 *	CAYUGA (LOCK 1), N.Y.	42 95	76.73	385	
D D	4 * 5	DDVDENE NEV	43.07	76 83	392	
	6	ITALY NY	42.47	76.32 77.28	1700 1020	
	7	NORTH LANSING, NY	42.62	76.53	870	
D	8	MACDOUGALL, N.Y.	42.82	76.85	675	
D	9 *	MACEDON (LOCK 30), N.Y.	43.07	77.30	466	
D	10 *	MAYS POINT (LOCK 25), N.Y	43 00	76 77	380	
D D	11 12 *	MEWADE (LOCK OR-B) NY	42 43	76.75 77.10	1430 434	
	13	PHELPS NY	42.03	77.10	640	
D	14	ELBRIDGE, N.Y	43 03	76.45	540	
D	15	SECOND MILO, NY	42 62	77.00	1050	
	16	SHELDRAKE, N.Y.	42 68	76.72	400	
D D	17 18 *	SYRACUSE (AIRPORT), N.Y.	42.77 43.12	76.60	1090	
-	19	SYRACUSE, NY S	42.93	76.12 76.17	419 420	
D	20	SYRACUSE, NY. SE	42.98	76.13	720	
	2١	GLEN HAVEN ROAD, N.Y	42 77	76.27	875	
D	22	HIMROD, N.Y.	42.57	76.97	1120	
	23 24	LOCKE, N.Y.	42.65	76.45	900	
		MANDANA, NY MARIETTA, NY	42.85 42.90	76.38 76.32	1080 810	
		MARTISCO, NY.	43.02	76.32	430	
D		NEW HOPE, NY.	42.80	76.35	1500	
		OTISCO VALLEY, N.Y.	42.80	76.22	880	
	29	RESERVATION, NY.	42.93	76.17	485	
	30 31	RICE GROVE, N.Y. SCHOOL NO. 10, N.Y.	42.85 42.80	76.25 76.38	800 1100	
		SKANEATELES, N.Y. GC	42.93	76.43	920	
	33	SPAFFORD, N.Y.	42.80	76.27	1720	
D		TRUMANSBURG, N.Y.	42.53	76.63	935	
		WATERLOO, NY. (LK CS-4)	42.90	76.85	450	
		EAST BLOOMFIELD, N.Y.	42.90	77.43	965	
		ITHACA, N.Y. AURORA, N.Y.	42.45 42.73	76.45 76.65	960 830	
		VICTOR	42.73		EST 500	
D !		FULTON (LK3)	MSG	NSG	MSG	
	<b>.</b> .	BARNES CORNERS, N.Y.	43.80	75.83	1390	
		BLOSSVALE, N.Y.	43.30	75.63	430	
_	J	CAMDEN 2.4 N (WOODS), N.Y.	43.38	75.73	745	

#### SNOW SURVEY STATIONS IN US, LAKE ONTARIO BASIN CAMDEN, N.Y. (FIELDS AND WOODS) 43.40 75.83 43.40 75.83 5 × 6 CASTOR HILL, NY 600 43 63 75.87 1350 43 62 75.77 1300 43.55 75.57 1660 43 43 75.75 880 Ε 7 × E. BRANCH, N.Y. 8 × FISH CREEK CLUB, NY. FLORENCE, N.Y. 9 × 10 \* GAYVILLE, NY. (WOODS) GREENBORO, NY. GMA GAYVILLE, N.Y. (FIELDS - WOODS) . 880 43.28 76.00 11 × GAYVILLE, NY. (WOODS) 470 43.28 76.00 12 \* GREENBORO, N.Y. 13 HAPPY VALLEY, N.Y. GMA 14 JAMISONS CORNERS, N.Y. 15 MALLORY, N.Y. (FIELDS AND WOODS) 16 MALLORY, N.Y. (WOODS) 17 MCCONNELLSVILLE, N.Y. 18 MEXICO N.Y. 43.63 75.88 1290 43.47 76.00 645 43.37 75.87 695 43.32 76.12 440 43.32 76.12 440 470 E MEXICO, N.Y MUNNSVILLE, N.Y. 18 £ 19 \* 43 45 76.23 470 Ε 20 × 42.97 75.58 720 42.92 75.82 1620 42.88 75.83 1440 43.33 76.00 550 43.58 75.75 1525 43.50 75.67 1340 21 \* NEW WOODSTOCK, (2.4N) N.Y. 23 \* N. CONSTANTIA, N.Y. 24 \* NORTH OSCEOLA, N.Y. 25 \* OSCEOLA, EAST, N.Y. 26 \* PANTHER LAKE, N.Y. 27 \* PETERBORO, N.Y. Ε Ε Ε Ē 43.32 75.90 630 Ε 42.98 75.73 1300 Ε 28 \* 42.90 42.95 PLEASANT VALLEY ROAD, NY 29 \* Ε 75.72 1340 29 \* POMPEY, NY 30 \* PRATTS HOLLOW, NY -∠.95 42.90 E 30 \* PRATTS HOLLOW, NY E 31 REDFIELD, N.Y. E 32 \* HIGHMARKET, NY E 33 \* SANDY POND, NY. E 34 \* STILLWATER DAM, NY E 36 \* TABERG, (1.5w) N.Y. (WOODS) E 37 \* TABERG, (3NW) NY. (FIELDS-WOODS) E 38 \* TABERG, (3NW) NY. (FIELDS-WOODS) E 39 \* THOMPSONS CORNERS, NY. (FIELDS) E 40 \* WEST MONROE, NY E 41 \* WILLIAMSTOWN, (185) NY.(FL-WD) E 42 \* WILLIAMSTOWN, (185) NY.(FL-WD) E 45 \* BREWERTON (LOCK 23), NY E 4 \* BIG MOOSE, NY E 4 \* 42.90 76.02 1680 42.92 75.58 1220 43.53 75.80 940 Ε NEW BREITAN, NY. BIG MOOSE, NY BOONVILLE (JACKSON HILL), NY. BOONVILLE, (1E) NY 43.83 75.38 820 43.82 74.87 1880 43.43 75.35 1600 43.47 75.30 1150 BRANTINGHAM, NY 1150 8 SEARS POND, NY 10 \* COPENHAGEN, NY 8 43 68 75 28 43 77 75 63 1700 43 87 75 63 1700 LOPENHAGEN, NY CROGHAN, NY CROGHAN CRO 43.87 75.68 1220 44.03 75.35 1000 43.77 74.72 1810 43.77 74.72 1810 43.45 75.07 1480 43.43 75.18 1180 HAWKINSVILLE, N.Y. 2E 43.50 75.23 1180 LOWVILLE, NY 43.78 75.48 MCKEEVER, N.Y 20 \* 850 43.62 75 10 1580 43.52 74.95 1820 43.87 75.18 1580 43.70 74.93 1810 43.57 75.25 1280 21 \* NORTH LAKE, N.Y 22 \* NUMBER FOUR, N.Y 01D FORGE, N.Y 24 OLD FORGE, N.T. PORTERS CORNERS, N.Y. 24 SEARS POND, NY 26 × 43.73 75.72 27 \* STILLWATER RESERVOIR, NY TURIN, N.Y. 1765 30 TURIN, N.Y. 43.90 75.05 31 \* WHITE LAKE (PURGATORY CAMP), NY 43.57 75.42 1 BARNUM POND, NY 43.57 75.13 2 \* BLUE MT. LAKE, NY 44.45 74.25 3 BAY POND, NY, \*24 44.45 74.42 4 SABATTIS, NY 44.10 74.67 43.90 75.05 43.62 75.42 75.42 1300 1550 1660 43.87 74.43 2220 74 42 1620 7467 BUCK POND, N.Y 1760 6 \* CARRY FALLS, NY. 7 \* CHASM FALLS NV 43.98 75.07 42.43 74.75 1780 7 \* CHASM FALLS, NY 8 \* CHATEAUGAY, NY 9 CHATEAUGAY, NY 1386 G 44.75 74.22 44 92 74.08 1050

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#### SNOW SURVEY STATIONS IN US, LAKE ONTARIO BASIN

		00.000		•		
G	11 *	CONIFER, N.Y.	44.22	74.62	1600	
G	12	DICKINSON, NY	44.75		1380	
G	13 *	CRANBERRY LAKE, NY	44.22		1500	
G	16 *	GALE, N.Y.	44.27		1700	
G	17 *	HARRISVILLE, N.Y.	44.18		760	
G	18 *	HORSESHOE LAKE, N.Y.	44.15	74.60	1800	
G	19 *	LITTLE TUPPER LAKE, N.Y	44.07		1720	
G	20 *	LONG LAKE, N.Y.	43.98		1760	
G	2	LAKE TITUS, N.Y.	44.72		1563	
G	22	MCDONALD POND, N.Y. #25	44.40		1580	
G	23	UPPER & LOWER LAKES, N.Y	44.60		300	
G	24	UPPER ST. REGIS, N.Y.	44.40		1630	
G	25	OWLS HEAD, N.Y.	44.70		1520	
G	26	PANTHER MTN, N.Y.	44.23		1645	
G	27	N BANGOR, NY	44.80		640	
G	28 *	PYRITES, NY.	44.53		400	
G	29 *	RAQUETTE LAKE, NY	44.23	74.75	1560	
G	30	STUDLEY HILL, N.Y.	44 67	74.22	1600	
G	31	SANTA CLARA, N.Y.	44.63		1600	
G G	32 *	SEVEY, NY	44.30		1540	
G	33	S. COLTON, N.Y.	44.43		1400	
G	34 *	STAR LAKE, NY	44 17	75.05	1500	
	35 36 *	GOODNOW MTN, N.Y	44.62	74 40	1700	
G G	37	TUPPER LAKE, NY.	44   2		1600	
G		TUPPER LAKE-KILDARE, NY.	44.25		1560	
G	39 ×	WANAKENA (8-SITE AVG.), N.Y	44.15		1510	
fram		CANTON	44.57	75.12 ES	ST 400	
4111	Classificati	Eggleson, Northeast Climate Center,	Cornell	University		

\* Classified as long-term station. Records available from 1968 to 1987

## Hydrometeorological Data Collection Design and Analysis for the Lake Ontario Drainage Basin

#### FINAL REPORT - PHASE I MAY 24, 1991

ATTACHMENT B

#### CANADIAN DATA BASE

#### **CLIMATE RECORDS**

#### **Daily Precipitation Records**

Records of monthly precipitation for all precipitation stations with long length of record in the Canadian drainage area have been furnished by Mike Webb (AES), Downsview, Ontario. A listing similar to the one for the U. S. climate stations is being prepared for the precipitation stations in the Lake Ontario drainage in Canada. No records of daily precipitation at Canadian stations have been requested or received.

Basically there are two type of stations in Canada that measures precipitation. One is the ordinary climatological station, at which the water equivalent of snowfall (the amount of precipitation as snow) is obtained by simply dividing the depth of freshly fallen snow by 10 (referred to as the 1 in 10 rule). The other type of station is a synoptic station. At synoptic stations the MSC Nipher snow gage, equipped with a solid wind shield, is used for measuring snowfall. At both stations, the official gage until the 1970-'s for measuring rainfall was the MSC standard copper gage. This is a round gage with a diameter of 3.568 inches, as area of 10 square inches, and installed with the gage orifice 12 inches above the ground.

During the 1970's the standard gage was changed to the Type-B rain gauge (Large Capacity). The Type-B gauge is 36 cm high, has is mounted with the orifice 40 cm above the ground surface. The gauge has a collecting funnel and outer container made of high strength plastic which minimizes adhesion of rain water on the gauge surface, and a clear plastic inner container, graduated for direct reading to the nearest 0.,2 mm. The total capacity of the gauge is over 250 mm, more than double that of the copper gage used previously.

The monthly precipitation values have been processed and placed in tabular form for each long-record station with annual, Oct-Apr and May-Sep totals and 30-yr average values (similar to the monthly form for the US stations). Missing records for stations with long records during the period 1960 to 1990 have been estimated from nearby stations.

Station history information on changes in location of stations are documented in the publication *Climatological Station Catalogue*, *Ontario*. A computer diskette of this publication has been furnished by Mike Webb (AES).

## Hourly Precipitation

Some Canadian climate stations are equipped with recording rain gages (mostly tipping bucket gages). However, only one precipitation amount is official for a location in Canada. Daily records of rainfall from tipping bucket gages are corrected to the rainfall measurement of the standard rain gage. Unless records of hourly and daily stations of precipitation at hourly stations are required, records from Canadian hourly stations will not be obtained. In the United States, different amount of precipitation for one from a non-recording gage).

## Temperature Records

Mean monthly temperature values for a large number of stations have been furnished by AES. No daily values of temperature have been requested at this time.

#### Wind

Average monthly wind speed records for periods up to 1988 have been furnished by AES for six synoptic stations. Records of daily winds for recent years for the synoptic stations in Canada have been furnished by Tim Hunter (GLERL), Ann Arbor, Michigan.

## SNOW SURVEYS

## Snow Surveys (Ground)

Historical snow survey records for 73 stations have been furnished by Peter Gryniewski, Ministry of Natural Resources, Toronto, Ontario. Records for an additional 15 stations in the Trent-Severn waterway have been furnished by Bruce Kitchen, Environment Canada, Park Service, Peterborough, Ontario. The earliest of these records began in 1957. The first and last pages of the tabular form of these records for the Lake Ontario drainage basin are shown in **Attachment B-1**.

Information as to location of each snow survey (elevation, latitude, longitude, and length of record) has been prepared and is shown in **Attachment B-2**. Diagrams of the area surrounding some of the snow surveys have also been received. These diagrams include detailed information as to the number of points in a survey and the relative location of the survey line to vegetative cover and terrain features and information on changes in snow survey locations.

## Snow Surveys (Airborne Gamma)

No airborne snow survey records are currently available for the Canadian portion of the Lake Ontario Basin. Locations for a new set of surveys in Canada have been selected by the NWS. Airborne gamma radiation surveys were conducted by Robert Grasty, Canadian Geological Survey in the early 1970s using airborne equipment that is now not available.

CANADA SNOW COURSE DATA, LAKE CNTARIO BASIN

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116 33.8 6.6 A F 130 31.1 7.4 A F 2 6 32.6 11.6 13.8 2.2 7 22 8.2 B F 3 6 29.2 8.2 D F 3 13 3.2 11.6 11.8 2.2 A F 130 31.1 7.4 A F 2 6 32.6 2.2 7 13.8 1.4 B F 3 6 7.6 1.6 D F 3 13 .2 1 1.6 13.2 3.1 A F 1 30 11.1 3.2 A F 2 6 9.3 1 1.6 15.5 3.7 A F 1 30 12.1 3.1 A F 2 6 9.3 1 1.6 15.9 3.2 A F 1 30 12.1 3.1 A F 2 6 12.8 A 11.6 16.9 4.1 B F 1 30 12.1 3.1 A F 2 6 12.8 A 11.6 16.9 4.1 B F 1 30 15.1 8.9 E F 2 6 10.9 2.2 7 17.7 3.7 A F 1 30 10 2.3 E F 2 6 10.9 11.6 15.9 4.1 B F 1 30 10 2.3 E F 2 6 10.9 11.6 2.3 4.3 B F 1 30 14.6 5.3 E F 2 6 10.9 11.6 2.3 4.3 B F 1 30 14.6 5.3 E F 2 6 10.9 11.6 2.3 4.3 B F 1 30 14.6 5.3 E F 2 6 10.9 11.6 2.3 4.3 B F 3 6 14.3 3.0 C F 3.1 3 0	SOIL CONDITION CODES FROZEN SOIL
25 4.5 B F 11.2 1.9 B F 11.2 1.5 B F 11.3 2 B F 11.3 2 B F 15.6 3.2 B F 15.6 3.2 B F 16.9 2.2 A F 10.8 1.3 B F 10.8 1.3 B F 16.5 2.6 B F 18.5 2.6 B F 18.5 2.6 B F 18.5 2.6 B F	IS CODES
ST-9 90 1.2 2  ST10 90 1.2 2  ST11 90 1.2 2  ST12 90 1.2 2  ST13 90 1.2 2  ST13 90 1.2 2  ST14 90 1.2 2  ST15 90 1.2 2	CRUST CONDITIONS CODES A NO CRUST B LIGHT CRUST

C CRUST STRONG ENOUGH TO HOLD A PERSON ON SNOWSHOES D CRUST STRONG ENOUGH TO HOLD A PERSON VAR VARYING

UD SOIL IS UNFROZEN AND DRY
UW SOIL IS UNFROZEN AND WET
THIS CODE IS FOLLOW BY A ZERO (0) TO INDICATE
THAT RESULTS ARE IN IMPERIAL UNITS (i.e. 1110\*)
OR BY A ONE (1) TO INDICATE THAT RESULTS ARE IN
METERIC (i.e. CM FOR SNOW DEPTH AND MM FOR WATER EQUIVALENT).

9

HYDEX MAY

FROM PETER GRYNEIWSKI - MINISTRY OF NATURAL RESOURCES ONTARIO, CANADA

ENVIRONMENT CANADA PARKS SER., PETERBOUROUGH, ONTARIO

FROM BRUCE KITCHEN -

28

CT1 +WILTEDOUED	_					HMENT B-2	2
STA #WATERSHED	SNOW COURSE NAME	BEG YR	YRS 91	EL(m)LAT	MINTO	NG MIN	
70 1 BRONTE CR WATERSHED	MORRISTON	7				80 5	
702 BRONTE CR WATERSHED	MOUNT NEMO	7		282 43	25	79 53	
801 OAKVILLE CR WATERSHED	KELSO	7		305 43	31	79 59	
901 CATARAQUI R WATERSHED 1001 BUELL CR WATERSHED	BATTERSEA	7	•	137 44	25	76 24	
1101 GANANOQUE R WATERSHED	BROCKVILLE	7		107 44	38	75 44	
1102 GANANOQUE R WATERSHED	DELTA	7		100 44		76 7	
1103 GANANOQUE R WATERSHED	GANANOQUE	8		106 44	_	76 15	
1104 GANANOQUE R WATERSHED	ATHENS	8	_	129 44		75 57	
1105 GANANOQUE R WATERSHED	OUTLET BLACK RAPIDS	8	-	107 44		76 4	
1106 MILLHAVEN CR WATERSHED	GOULD LAKE		-	114 44		76 6	
1107 LITTLE CATARAQUI WATESHED	KINGSTON	9	-	150 44		76 36	
1201 CREDIT R WATERSHED	BELFOUNTAIN	9) 7:		120 44		76 30	
1202 CREDIT R WATERSHED		7		<b>3</b> 66 43		80 1	
1203 CREDIT R WATERSHED	MONORA (ORANGEVILLE) TERRA COTTA	6:	_	427 43 343 43		80 6 79 57	
1204 CREDIT R WATERSHED	HILLSBURGH	7:		480 43	48	80 10	
1205 CREDIT R WATERSHED	MEADOWVALE	8		166 43		79 44	
1301 CROWER WATERSHED	CARDIFF	7		357 44		77 58	
1302 CROWER WATERSHED	COE HILL	7	· · ·	326 44	51	77 53	
1303 CROWER WATERSHED	CORDOVA	7		202 44	_	77 48	
2301 HUMBER R WATERSHED	ALBION HILLS	5		268 43		79 50	
2302 HUMBER R WATERSHED	COLD CR	79	9 11	268 43		79 42	
2303 HUMBER R WATERSHED	CLAIREVILLE	79	11	168 43		79 40	
2304 HUMBER R WATERSHED	BOYD	78	3 12	165 43		79 35	
2305 DUFFIN CR WATERSHED	CLAREMONT	78	3 11	180 43	50	79 5	
2306 DUFFIN CR WATERSHED	STOUFFVILLE	79	11	268 43	58	79 14	
2307 ETOBICOKE CR WATERSHED 2308 ROUGE R WATERSHED	HEART LAKE	7 9		253 43	45	79 48	
2401 SPENCER CR WATERSHED	BRUCE'S MILL	79		256 43	57	79 21	
2402 SPENCER CR WATERSHED	CHRISTIES CORNERS	73	· -	241 43	i 7	80 2	
2403 SPENCER CR WATERSHED	FIDURI ALBIUN	//	· <del>-</del>	183 43		79 50	
2404 SPENCER OR WATERSHED	VALENS	70	=	274 43		80 8	
2701 MOIRA R WATERSHED	DUNDAS VALLEY MADOC (O'HARA)	71	_	145 43		80 1	
2702 MOIRA R WATERSHED	ACTINOLITE (DDICES)	59		198 44		77 31	
2703 MOIRA R WATERSHED	ACTINOLITE (PRICES) PLAINFIELD (HOSKIN'S)	59		167 44		77 20	
2704 MOIRA R WATERSHED	STIRLING (SPRACKETT'S)	59 60		107 44 190 44		77 21	
2704 MOIRA R WATERSHED 2705 MOIRA R WATERSHED	MILLBRIDGE	79		190 44 305 44		77 30	
2706 MOIRA R WATERSHED	HAWKINS BAY	84		168 44		77 35 77 19	
2707 MOIRA R WATERSHED	LIME LAKE	84		160 44		77 19 77 10	
2901 NAPANEER WATERSHED	SECOND DEPOT LAKE	73		168 44		75 24	
2902 NAPANEE R WATERSHED	FOURTH DEPOT LAKE		-	168 44		75 24 76 47	
JIUI UIUNABEER WATERSHED	SQUIRREL CR	72		190 44		75 20	
3201 INDIAN R WATERSHED	WARSAW	72		235 44		76 5	
3801 TRENT R WATERSHED	CAMPBELLFORD (SEYMOUR)	76		137 44		77 48	
3802 TRENT R WATERSHED	HUNTINGDON (SILLS)	76	14	143 44		77 27	
3803 TRENT R WATERSHED	ORLAND (LOOMIS)	76	14	137 44		77 49	
3901 BUTLER CR WATERSHED	BRIGHTON (PROCTOR)	76	14	151 44		77 45	
4001 WELLAND R WATERSHED	MOUNT HOPE	73	16	216 43	8 7	79 56	
4002 WELLAND R WATERSHED	SOUTHCOTE	73	12	240 43	11 7	79 57	
4003 WELLAND R WATERSHED	WAINFLEET (WINGER)	78		177 42	56 7	9 27	
4004 WELLAND R WATERSHED 4005 WELLAND R WATERSHED	BINBROOK	84	6	213 43	7 7	79 51	
4006 BLACK CREEK	CHIPPAWA	84	б	180 42	59 7	9 31	
4007 FOUR MILE CREEK	STEVENSVILLE	84	0	180 42	56 7	'9 4	
4101 BLACK R (L'ONTARIO DRAINAGE)	VIRGIL	90	0	96 43		9 7	
4102 DEMORESTVILLE CREEK WATER	DEMODESTALLS COSE	85	5	98 43		7 6	
4103 CONSECON CREEK WATERSHED	CONSECON CREEK	85	5	107 44		7 12	
4104 LANE CREEK WATERSHED	LANE CREEK	85	5	110 44		7 18	
4105 BLOOMFIELD	BLOOMFIELD CREEK	85	5	91 43		7 19	
4106 MARSH CREEK WATERSHED	MARSH CREEK	85 85	4	96 44		7 13	
4601 COBOURG R WATERSHED	HARWOOD	85 79	5	116 44		7 8	
4602 COBOURG R WATERSHED	CAMBORNE	79 80	11	297 44		8 10	
4603 GRAHAM CR WATERSHED	STARKVILLE	80	10 10	229 44 168 43		8 11	
4701 LYNDE CR WATERSHED	ASHBURN	79	10	267 44		8 31 9 1	
4801 OSHAWA CR WATERSHED	MOUNT CARMEL	79	9	267 44		9 1 8 53	
4802 OSHAWA CR WATERSHED	RAGLAN PURPLE WOODS	82	9	305 44		8 56	
4901 BOWMANVILLE CR WATERSHED	STEPHEN'S GULCH 1 CON 111	79	ğ	144 43		8 42	
4902 BOWMANVILLE CR WATERSHED	STEPHEN'S GULCH 2 CON IV	79	10	146 43		8 41	
					-0 /	· 1	

	CANADIAN SNOW COURSES, LAKE C	FONTADIO BACILI	
4903 BOWMANVILLE CR WATERSHED 6801 BALSAM LAKE WATERSHED 6802 STURGEON LAKE WATERSHED 6803 PIGEON R (KAWARTHA L.) 6804 MARIPOSA BROOK WATERSHED FROM PETER GRYNIEWSK	COMO SAULT COBOCONK CAMERON PONTYPOLL WOODVILLE	81 10 312 44 3 78 87 4 265 44 38 76 87 4 250 44 24 78 91 4 275 44 8 76 91 0 264 44 23 79	50 46 41
ST-1 EAGLE LAKE ST-2 LITTLE BOB LAKE SY-3 FURNACE FALLS ST-4 BEAR LAKE ST-5 CARNARVON ST-6 BALSAM LAKE PROV. PARK ST-7 SIBBALD POINT PROV. PARK ST-8 SERPENT MOUNDS PROV. PARK ST-9 EEL'S LAKE ST 10 STONY LAKE ST 11 LITTLE BRITAIN ST 12 EMILY PROV. PARK ST 13 COOPER'S FALLS ST 14 SCANLON CREEK CONSV. AREA ST 15 GILCHRIST  FRCM BRUCE KITCHEN,	TRENT-SEVERN WATERWAY	77	24

# Hydrometeorological Data Collection Design and Analysis for the Lake Ontario Drainage Basin

#### FINAL REPORT - PHASE I MAY 24, 1991

ATTACHMENT C

#### ADJUSTMENT TECHNIQUES FOR PRECIPITATION RECORDS

#### **NEED FOR A KNOWLEDGE OF ACTUAL PRECIPITATION**

Hydrologists have long recognized that deficiencies exist in precipitation measurements, especially when it occurs in the form of snow. Errors in measurement of precipitation account for a large portion of the inaccuracies in precipitation-runoff and in hydrological modeling of runoff or lake inflow. A considerable effort has been devoted by scientists around the world on the development of techniques and instrumentation for improvement in the measurement of precipitation. The use of conceptual modeling has greatly increased the need for improved knowledge of the amount and distribution of the actual precipitation, rather than an index to the amount. Beside the need for improved knowledge of the actual amount of precipitation for hydrological modeling, this knowledge is also needed for accurate assessment of the total deposition of acid rain and other environmental and hydrometeorological modeling of the atmosphere and lithosphere.

#### **ACCURACY OF PRECIPITATION SENSORS**

Many investigators, Kurtyka (1), Israelsen (2), and Larson (3) have presented reviews of the various instruments and techniques developed over the past 100 years to improve the measurement of precipitation. The World Meteorological Organization (WMO) published a comprehensive review of the many problems associated with precipitation measurement in the WMO/IHD Report No 16, The Precipitation Measurement Paradox -- The Instrument Accuracy Problem, by Rodda (4). All of the above reports agree that there is a deficiency in the measurement of precipitation which is normally much greater for snowfall than for rainfall and that the deficiency in the catch is primarily the results of wind action and turbulence around and over the orifice of the gaging instrument. Other sources of error in precipitation measurement are the result of loss due to wetting of the gage and, especially for areas where most precipitation is light and in the form of snow, the loss by not accounting for precipitation during periods when a trace (< 0.005 inch in the U.S. and < 0.2 mm in Canada) is recorded.

Many different types of precipitation gages and devices to protect precipitation gages from the adverse effects of wind have been developed. The most common has been the development of wind shields to reduce the adverse effects of wind movement at the gage orifice. The use of windshields, for gage sites where wind is a factor, does result in a gage catch which is normally greater than that without the use of a windshield, but which is still less than the true amount of precipitation.

## **EXPOSURE OF PRECIPITATION GAGES**

Bogdanova (5) showed that in a well protected site, such as in a small opening in a large coniferous type forest, the catch in a precipitation gage does provide a fair indication of the average snowfall in the surrounding area. Similar research was conducted by this author and other NWS personnel at the Sleepers River Watershed near Dansville, Vermont. In this research, many types of precipitation gages (with and without windshields) were installed in a site in a small forest clearing. The site was protected from wind movement by a wall of black plastic entirely surrounding the site, extending from the ground to near the top of the trees (referred to as the black hole). Analyses of the amount of precipitation measured in the various precipitation gages showed that there were essentially no differences in the measured precipitation (for both snowfall and rain). The precipitation as measured in the precipitation gages related one to one with the water equivalent of the snowfall for the same storm period as measured in the protected site and as estimated from many precipitation and snow survey measurements in the research area. An anemometer installed in the black hole verified that there was no wind movement in the protected site.

The conclusions of this research supported the findings of Bogdanova and others that under no wind conditions all precipitation gages, with and without a windshield, measures the same amount of precipitation and that the measurements reflect the actual precipitation that is received at the ground surface. However, no gage in the real world is so protected from adverse wind effects and catches in almost all gages measure less than actual precipitation, especially for snowfall. The measurement problem is also compounded by the fact that under the same wind conditions, different gages will measure a different proportion of the actual precipitation.

The results of research by Brown and Peck (6) demonstrated that the exposure of a gage site, or the degree of protection afforded a precipitation gage from adverse wind movement by surrounding objects, is the most important factor relating to the accuracy of a gage in measuring true precipitation. Brown and Peck (6) developed a subjective exposure classification system, based on the degree of protection afforded by nearby objects and by the general terrain near the gage. This system was used in a snowfall measurement project by the NWS to classify precipitation gage sites in the Lake Ontario drainage area during the International Field Year for the Great Lakes (IFYGL) in the early 1970s (7). The Brown and Peck subjective classifications of exposure, in order of protection provided by nearby objects and the general terrain,

are:

- 1. Well-protected. Sheltered in all directions by objects subtending angles of 20° to 30° from the gage orifice with none greater than 45°, and with objects of sufficient breadth to minimize edge effects. As example of a well-protected site is an open area in a large coniferous forest, where the vegetation provides maximum protection the year around. The gage should not be located so that strong winds would be funneled into the area by the surrounding terrain.
- 2. <u>Protected</u>. Sheltered by the general terrain of the area but not fully protected from wind action on the gage by objects in the vicinity. The unprotected directions should not be in the general direction of the winds associated with precipitation.
- 3. <u>Fairly well-protected</u>. May or may not be sheltered by the general terrain. Nearby objects provide some protection from winds associated with major storms. The precipitation catch would be reduced during snow storms with strong general winds.
- 4. <u>Moderately windy</u>. Little protection by the general terrain. Nearby objects do not have the expanse or breadth to afford adequate protection from winds during periods of precipitation.
- 5. Windy. Little or no protection from nearby objects but the location may have some protection afforded by the general terrain.
- 6. <u>Very Windy</u>. No protection from the general terrain, or the general terrain is such that the location is subject to stronger winds that found in the area. Little or no protection from nearby objects. Examples would be gages exposed on mountain tops or ridges or at the mouth or head of canyon where strong winds might be funneled to the site. Both "windy" and "very windy" locations have very open exposures. The difference is that a "very windy" location is subject to adverse effects because of the general terrain.
- 7. Overprotected. One or more objects in the vicinity of the gage extending an angle of more than 45° in the vertical, with that portion of the object or objects extending above 45° having a horizontal angle greater than 10°.

#### **NEED FOR ADJUSTMENT OF PRECIPITATION RECORDS**

A report prepared by Walter Wilson (8) published in the Monthly Weather Review presented an excellent case for using precipitation records that are as near as possible to the actual amount of precipitation for hydrological modeling. His report clearly demonstrated that precipitation records from stations having a good exposure, i. e., protected from strong wind movement, had a much higher correlation with streamflow that did records from stations which were poorly exposed, i. e., open to wind movement.

Hydrologists of the National Weather Service (NWS) have used correction factors to adjust precipitation records when using precipitation records for conceptual hydrological modeling. These adjustments, or corrections, usually takes the form of a simple multiplying factor greater than unity to be applied to snowfall measurements. For basins with a major

contribution from snowmelt, the National Weather Service River Forecast System (NWSRFS) permits the calculation of a snow correction factor (SCF) for correcting precipitation in the form of snow during the calibration of its snowmelt model to a snowmelt basin. Larson and Peck (9) demonstrated that for bulk input (single precipitation value for the basin) conceptual modeling that include snow-accounting processes provide better simulation results if the wind induced snow precipitation measurement error is reduced through the use of an SCF.

Many users assume that precipitation data collected by, and published by, a national hydrometeorological organization, such as the NWS in the United States and the AES in Canada, are collected using standard criteria. This is not true for equipment in the United States. It is especially not true for exposure of precipitation gages in both countries. Since the most critical factor affecting the accuracy (and deficiency) of precipitation measurement is one may think that the exposure of a gage for measuring precipitation occurrence, consideration for location of a precipitation gage. However, this is not the case. Unless adjustments of precipitation records are made to correct for adverse wind effects and other errors in precipitation measurement, the use of published precipitation values for conceptual hydrological modeling, without proper consideration for measurement errors, will be misleading.

## ADJUSTMENT PROCEDURES - UNITED STATES

The US precipitation gage records will be adjusted by procedures developed by Hydex. One adjustment is based on a knowledge of the exposure of the gages to determine the gage catch deficiency as a result of wind action. The daily records of the observers who operate the gages will be used to account for losses due to wetting of the gage and for the loss in catch when a trace amount is reported. A trace of precipitation is considered as zero amount of precipitation in both Canada and the United States. The procedures are based on research work by the World Meteorological Organization WMO, the NWS, scientists in the USSR, scientists of the AES in Canada, and by many other investigators.

## Adjustments at Synoptic Stations

Larson and Peck (9) used information from many foreign and U. S. research reports, from research accomplished by the NWS at the Sleepers River Watershed in Danville, Vermont, and from studies conducted by the NWS and the U. of Wyoming near Laramie, Wyoming, to develop generalized curves for adjusting daily precipitation measurements for synoptic weather stations in the eastern United States. Wind sensors at synoptic stations (most are at airports) are generally installed at 20 feet above the ground. To determine the wind at the orifice level of the precipitation gage, the wind values from the wind sensors are reduced to the height of the precipitation gage orifice using the power-law profile,

$$U_{\text{gage}} = U_{\text{wind}} \left( \frac{Z_{\text{gage}}}{Z_{\text{wind}}} \right) , \qquad (1)$$

where  $U_{\text{gage}}$  is the daily wind movement at the gage height,  $U_{\text{wind}}$  is the daily wind movement as measured at height of the anemometer,  $Z_{\text{gage}}$  is the height of the precipitation gage,  $Z_{\text{wind}}$  is the height of the wind anemometer, and k a power. The value of k is dependent upon the stability of the atmosphere near the ground and on the roughness of the surface. A value of 1/7 for k in equation 1 is suggested in the book Hydrology for Engineers (10). A computation of k values at NWS synoptic stations using observed wind values at two levels (mainly 20 feet and 2 feet) indicated a value of 0.3 for k (unpublished report by the Hydrologic Research Laboratory NWS, Silver Spring, MD). Atmospheric conditions are generally most stable during the cold season when snow occurs. Since snowfall is the most important form of precipitation to be adjusted, and to be conservative, a value of 1/5 for k has been used by Hydex in the past. Before finalizing a value for k for the present project, more investigation will be conducted. The difference in estimated gage deficiency from using a 1/5 value compared with using a 1/7 value is small.

Figure C-1 shows curves, adapted from Larson and Peck (9) for obtaining the deficiencies in the daily catch in a precipitation gage based on the average daily wind speed (in mph) for:

- a. Rain
- b. Snowfall (with a windshield)
- c. Snowfall (without a windshield)

The relationship in Figure C-1, and those in Figures C-2 through C-9, were developed during an analysis study for the Environmental Protection Agency (EPA) to provide a consistent and reliable precipitation data set for evaluation of acid rain deposition simulation models (11).

The rain curve in Figure C-1 is used to determine the deficiency in the daily catch due to wind effects when the precipitation is in the form of rain. Synoptic stations in the northeast area of the United States are usually equipped with a shielded recording gage (which is used for the official precipitation measurement) and therefore the middle curve (Snow with windshield) is used for US synoptic stations in the Lake Ontario area when snowfall occurs.

At synoptic stations, the type of precipitation is generally reported each day. For mixed forms of precipitation at synoptic stations, rain and snow or other combinations of frozen precipitation with rain, the average of the deficiencies determined using (a) the rain curve, and (b) the snow with windshield curve, from Figure C-1 is used. Mixed forms of precipitation most often occurs when the daily average air temperature is between 27° F and 32° F.

## Adjustments at Climate Stations

Wind measurements are very seldom available at daily climate stations. A few stations that measure pan evaporation normally report wind movement at the height of the

evaporation anemometer (about 2 feet) but only during the warmer months of the year. Therefore, some method is needed to determine the wind adjustment factor to adjust daily or monthly precipitation totals from climate stations.

One method would be to estimate the daily or monthly wind movement at the height of the gage orifice from available wind measurements in the area. A research study was conducted by the author (unpublished) using hourly recording wind records from NWS synoptic and from U. S. Forest Service Ephraim Research experiment stations in Utah. Average hourly, daily and monthly wind speed values were correlated for stations located along the western side of the Wasatch mountains that traverse north-south through the central portion of the State. The interesting result of this study was that records of average daily (and monthly) wind speeds were well correlated (r greater than 0.85) for pairs of stations where wind measurements were made in the open, i. e., at airports where the wind measurement is made at open exposures with little or no protection from the wind. This was true for sites on the same side of the mountain range even as far as 175 to 250 miles apart (Salt Lake City to Milford and Salt Lake City to Modena, Utah).

A good correlation was also found between wind movement at the Salt Lake City airport (4,200 feet) and at open sites at the Ephraim Research area high in the mountains (over 9,000 feet). Little or no linear correlation was found between wind records for measuring sites only a few hundred feet apart when one of the sites had an open exposure and the other was located in an area protected by trees and bushes.

The results of the research demonstrated that a measure of wind speed in an open site can be used to estimate the wind speed in other open sites over considerable distances for locations not separated by mountain ranges.

Wind records for the synoptic stations in the Lake Ontario basin were analyzed to determine if these records were correlated on a daily or monthly basis as was observed in Utah. It was found that average wind speeds at Buffalo and at Rochester, New York, correlated well for both daily and monthly periods (r² approximately 0.78). Figure C-2 is a plot for Buffalo and Rochester of average monthly wind speed (for 12 winter months in 1989 and 1990). Figure C-3 is a plot of average wind speed for the two stations for February-March 1989.

Analysis of the correlation between average wind speed at Syracuse with those at Rochester were not as well correlated (r<sup>2</sup> approximately 0.65). This was expected since the Syracuse Airport is more protected from general wind movement by the local terrain and vegetation in the area and the wind sensor is not as open to wind movement as are the wind sensors at Rochester and Buffalo.

Since there is a high correlation for both daily and monthly periods between the average wind speed at Buffalo and Rochester, it is possible to estimate the average daily or monthly wind speed for other precipitation stations installed at open sites around Buffalo and Rochester. Daily adjustment factors may be determine for precipitation station records at open sites using estimated wind speed values and the curves in Figure C-1.

During the initial development of the adjustment techniques for EPA (11), daily precipitation records were adjusted for other synoptic stations at open exposures in the eastern United using Figure C-1 and the daily adjusted values were summed to obtain monthly adjusted values. The monthly adjusted values were compared with observed

values to compute monthly adjustment factors. These computed monthly adjustment factors were used to prepare the topmost curve (for windy sites) in Figure C-4 (For Computation of Deficiency in Catch of Rain, U. S. Precipitation gages). No data are available for developing a curve for "very windy" sites for Figures C-4. Very windy sites are generally found on and near higher mountains than exist in the Lake Ontario drainage area.

## Adjustment for Other than Windy Sites.

Most climate stations are located at sites that are partially, or in some cases very well protected, from wind movement. The wind movement at such sites is less than occurs at open sites. A means of estimating the daily or monthly wind movement at these less windy site is needed.

The curves for rain measurement for exposures other than windy in Figure C- 4 have been arbitrarily assigned as percentages of the windy curve as follows: moderately windy, 0.75%; fairly-well protected, 0.50%, protected, 0.25; and well-protected 0.0%. No curve is given for the classification Overprotected since these are rarely found (substation network specialists in the US who install gages are instructed to avoid such locations) and the deficiency in catch is not much different in most cases than that for well-protected sites.

Sets of curves for use with snow measurements for gages with and without snowfall, similar to the curves for rain in Figure C-4, are needed. The curves for windy exposures on Figure C-5 (for US gages without windshields) and Figure C-6 (for US gages with windshields) were developed using precipitation and wind measurements from synoptic stations as was done for computation of the windy curve in Figure C-4.

The positioning of curves for the other exposure classifications on Figures C-5 are based on the relative deficiencies found for the different exposure classifications for the same wind speeds as reported in the paper by Brown and Peck (6).

The curves for deficiency in snowfall catch for gages without windshields (Figure C-6) have been adjusted upwards from those in Figure C-5 using on the results of research reported in the literature comparing the deficiencies of catch of snowfall with and without a windshield.

The basic assumption for the use of the curves in Figures C-1, C-4, C-5 and C-6 is that wind measurements at a windy site represents the wind movement in the general area. The wind movement for the open site can be estimated using wind records from nearby windy locations. For less open sites, the wind movement should be proportionally lower, depending upon the amount of protection offered to the precipitation by the vegetative cover and by terrain features.

## Adjustment for Cases of Mixed Forms of Precipitation

When the curves for monthly adjustment of precipitation are used the following criteria are used to determine when to use the rain (Figure C-4) or snow curves (Figures C-5 and C-6), or an average of the two deficiencies:

Average Monthly Temperature (T)
Rain T > 28° F
Snow T < 24° F
Mixed 24°F = T = 28°F

# Assignment of Exposure Classification for a Gage Site.

The use of an exposure classification system would not be required if wind speed were measured at each precipitation gage site. However, technicians and scientists can be readily trained to use the system to determine a proper exposure classification for a site. As indicated in the this report, the Brown and Peck (6) exposure classification system was used during the installation and evaluation of gage sites in the Lake Ontario drainage area during the IFYGL studies in 1973 and 1974. It was found that with experience the Substation Network Inspector for New York at that time (Donald L. Quick) came up with essentially the same classification of sites as this author. Subsequently, prior to his retirement, Donald Quick produced many detailed diagrams documenting on the station history forms for precipitation station locations in the State of New York that are excellent for use in defining the exposure of stations in the Lake Ontario area.

Stations history files are available at the Washington NWS offices. Copies of station history forms for all stations listed in Attachment A-1 of Attachment A have been obtained.

# Adjustment for Wetting of the Gage and for Traces

It has been the practice of Hydex to correct for trace days at climate and synoptic stations by adding a 0.005 inch to the total precipitation for the month for each day a trace amount is reported. Goodison (12) has shown that a correction for wetting of a gage when the amount of precipitation is measured is required for type MSC Canadian precipitation gage since the liquid is poured from the gage for the observation. For the MSC gage Goodison has proposed a wetting correction of 0.07 mm per observation (or 0.25 mm per day). The new Type-B rain gage has a measurement tube that is transparent and the measurement is made visually. This gage does not require the liquid to be poured from the gage. A wetting correction for the US standard 8-inch raingage is not as important since the liquid is not poured from the gage for rain measurement but measured using a wooden stick.

Goodison has also recommended a correction value of 0.15 mm for each observation a trace is reported (personal communication).

## ADJUSTMENT PROCEDURES - CANADA

# Adjustment of Daily Measurements for Synoptic Stations

Measurement of precipitation at synoptic stations in Canada is done separately for rain and snowfall. Rain is measured using the Type-B standard gage. A search of the literature did not produce a curve relating gage deficiency with wind movement for the Type-

B gage but measurements are being compared with pit gage rainfall for this purpose. The available information on catch deficiency of rain gages with diameters smaller than 8 inches is not consistent. Huff (13) reported that there were small differences in catch or rain for a three-inch orifice gage and a standard 8-inch gage. Unpublished studies by the NWS, at the Danville, Vermont, Sleepers River Watershed snowmelt study site, indicated that the deficiency for rain catch by a four-inch gage was about half that for an eight-inch gage with 4 to 5 mph wind movement (ground truth pit gage measurements were used in the comparison study). Goodison (private communication) of AES Canada has indicated that the average catch deficiency for rain is on the order of 4 to 5 percent using the MSC standard copper gage. Goodison has reported that preliminary comparison with pit gage measurements indicates that the catch deficiency for the Type-B gage is on the order of 2%.

Based on the evidence available, the gage catch deficiency for the Canadian standard rain gage for this project will be considered to be one-half of the deficiency for an eight-inch rain gage (one-half of the deficiencies determined using Figure C-1).

For measurement of snowfall at synoptic stations in Canada the MSC Nipher snow gage is used. This is equipped with a solid wind shield. Goodison (12) has shown that for light winds (up to 5.5 mps), the Nipher gage measurements are within 10 percent of estimated true snowfall, with the catch being slightly above true snowfall for wind speeds from 1 to 4 mps. Figure C-7 (Effect of Wind Speed on Catch of Canadian Nipher Snow Gage) has been adapted from Goodison (12) and shows the relation of the gage height average daily wind speed and the deficiency in catch for the Nipher gage for measurement of snowfall.

Wind measurements are available at some Canadian synoptic stations which are equipped with the Nipher snow gage. For these locations the only calculation required for using Figures C-1 to determine the deficiencies in catch due to wind is to reduce the wind speed from the height of the anemometer to the height of the orifice of the precipitation gages. For other stations with Nipher gages wind movement is not recorded. It will be necessary to estimate daily wind speed values from other nearby synoptic stations that record wind as described in the previous section, Adjustment Procedures - United States.

Daily precipitation records for Canadian Synoptic stations during the period they are equipped with a Nipher snow gage will be adjusted using Figure C-7 for snowfall and one-half of the deficiencies determined using Figure C-1 for rain. In addition to these corrections for wind effects, corrections will also be made for losses from wetting of the Nipher gage and for days a trace of precipitation is reported. An amount of +0.15 mm for each time the liquid is poured from the gage to a graduate for measurement will be used for the correction for the wetting loss. A correction values of +0.07 mm for each day a trace is reported for the Nipher snow gage.

## Adjustment for Monthly Precipitation Values for Synoptic Stations

Not all stations have had Nipher gages for the full data base period, 1961-1990. Synoptic stations prior to the use of the Nipher gages were equipped with the MSC standard rain gages for rainfall and the 1 to 10 rule was used for snowfall. Figure C-8 (For Computation of Deficiency in Monthly Catch of Rain, Canadian Standard Rain Gage) was

developed from wind and precipitation data for many synoptic stations by computing daily adjustment values and summing for monthly totals. For stations without wind measurement, or for periods without wind measurement, the monthly wind will be estimated from nearby stations following the procedures outlined in the previous section, Adjustment Procedures - United States.

Figure C-9 (For Computation of Deficiency in Monthly Catch of Snowfall, Canadian Nipher Gage) was developed by Hydex from synoptic station data for the southeastern areas of Canada, similar to the development of Figure C-8. From the two curves of Figure C-8 it is evident that the wind movement adjustment for stations in the Maritime Climate of the eastern provinces of Canada is much less than for locations in the colder and drier climate of Ontario and Quebec.

## Climatological Stations Using the 1 to 10 Rule

No technique has been found in the literature for adjusting snowfall measurements using the 1 to 10 rule. Prior to 1960 all AES stations used this method of measurement. Goodison (14) has shown that this method can be subject to substantial error. As for other measurement methods the exposure of the measurement site where the measurement is made is also a factor in how well the method measures the true precipitation. Studies by the NWS at Danville, Vermont, showed that the accumulation of snow on a snow board, or on an area cleaned for measurement of the depth of the snowfall, varied considerably in respect to the true snow fall for different exposure. During the snow measurement studies at Danville, Vermont, NWS researches found that the snow on the ground during a period of snowfall, even in a fairly well-protected site, was observed to move towards the perimeter of a small open area even with very low wind speeds (2 to 3 mph). This complicate the comparison of a snowfall measurement with snow survey data or snowfall measurements and was the primary reason the "black hole" (discussed in the section Exposure of Precipitation gages) was created to provide a truer measurement of the actual snowfall at Danville, Vermont.

No adjustments are planned for precipitation records from the Canadian climatological stations using the 1 to 10 rule. These records will be tested for consistency.

For those synoptic stations having periods of records where the 1 in 10 rule was used prior to the installation of a Nipher gage and the location of the measuring sites have not changed, an indication of required adjustment for the 1 to 10 rule observations of precipitation in the form of snow may be developed. However, because of the effect of different exposure, the adjustment factors may not be universally applied without more data and research.

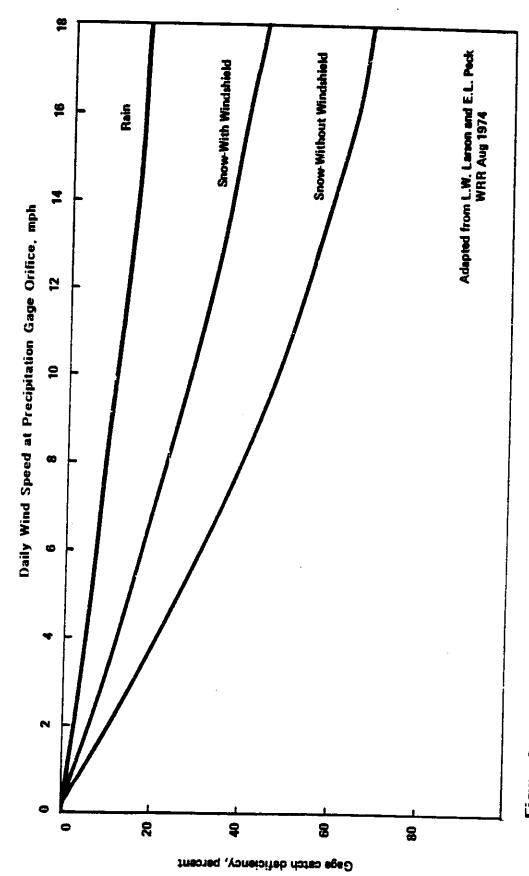


Figure C-1 EFFECT OF WIND SPEED ON CATCH OF U.S. PRECIPITATION GAGES

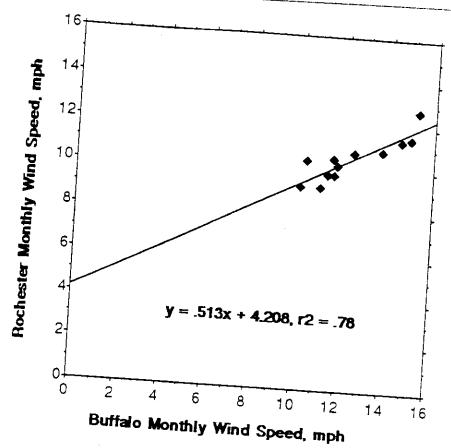


Figure C-2 Average Monthly Wind Speed - Rochester vs Buffalo, 1989-90

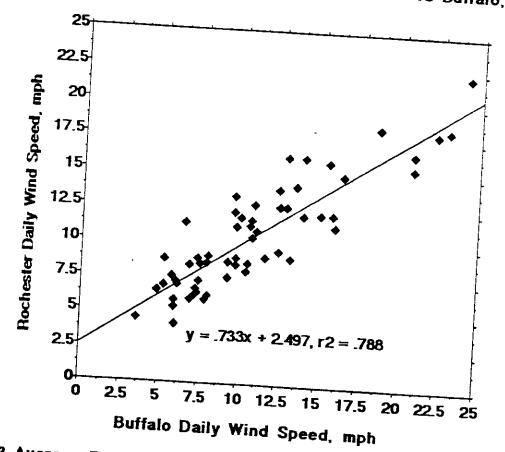


Figure C-3 Average Daily Wind Speed - Rochester vs Buffalo, Feb-Mar 1989.

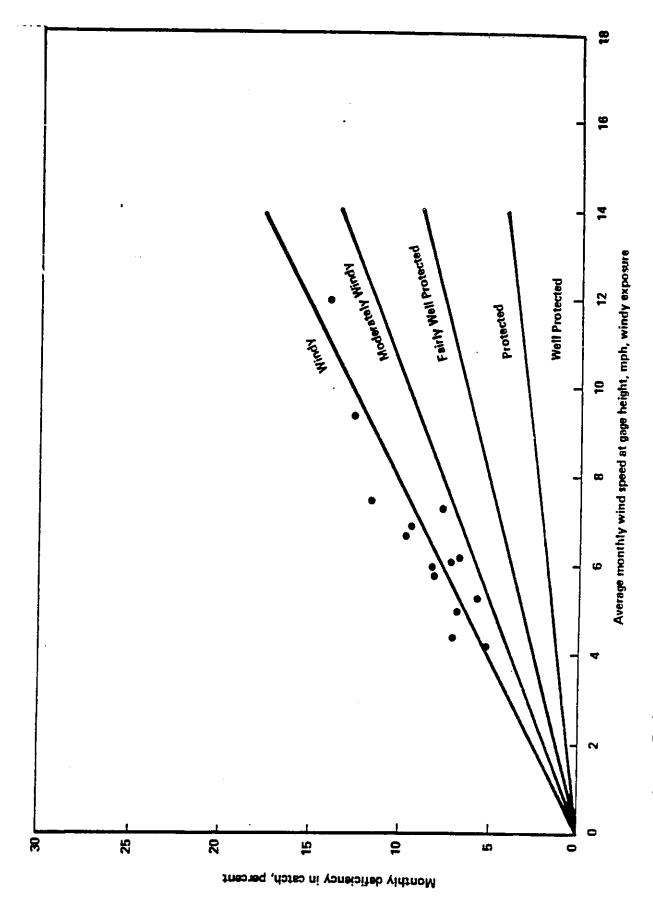
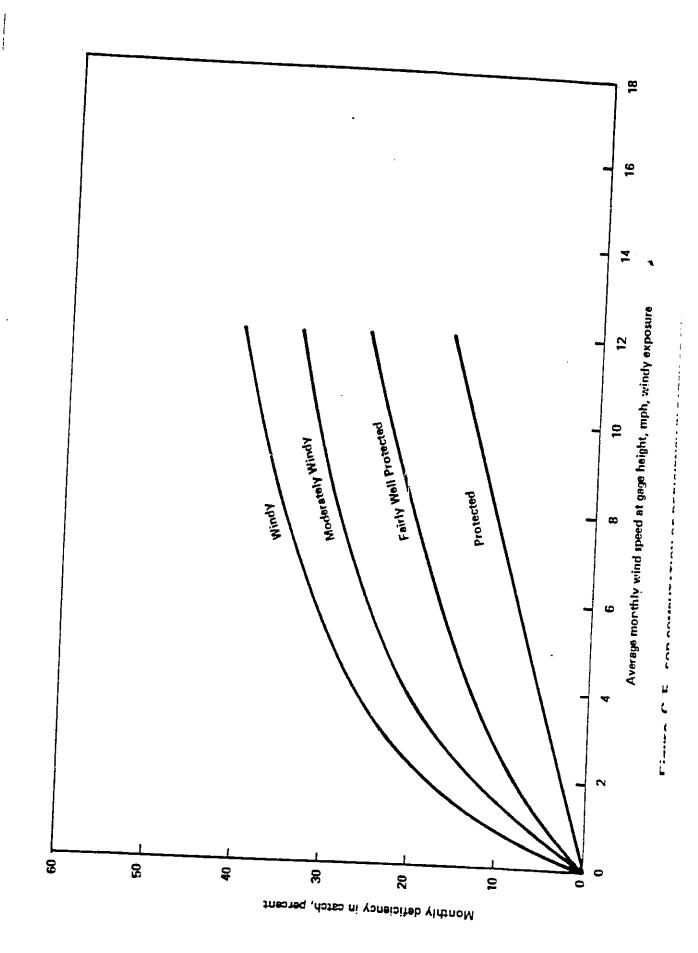
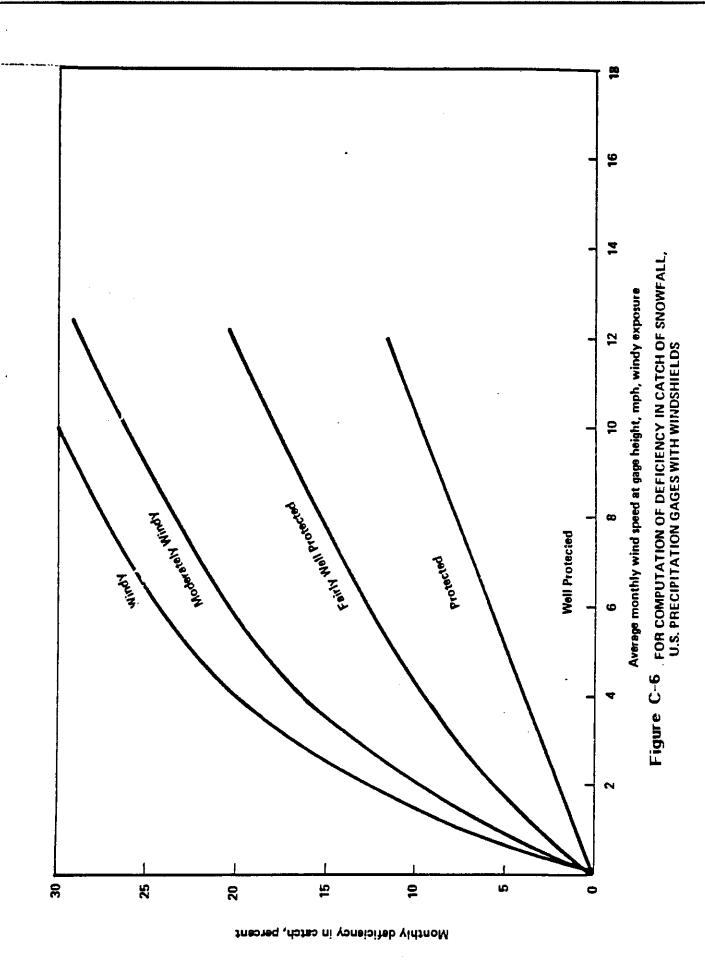
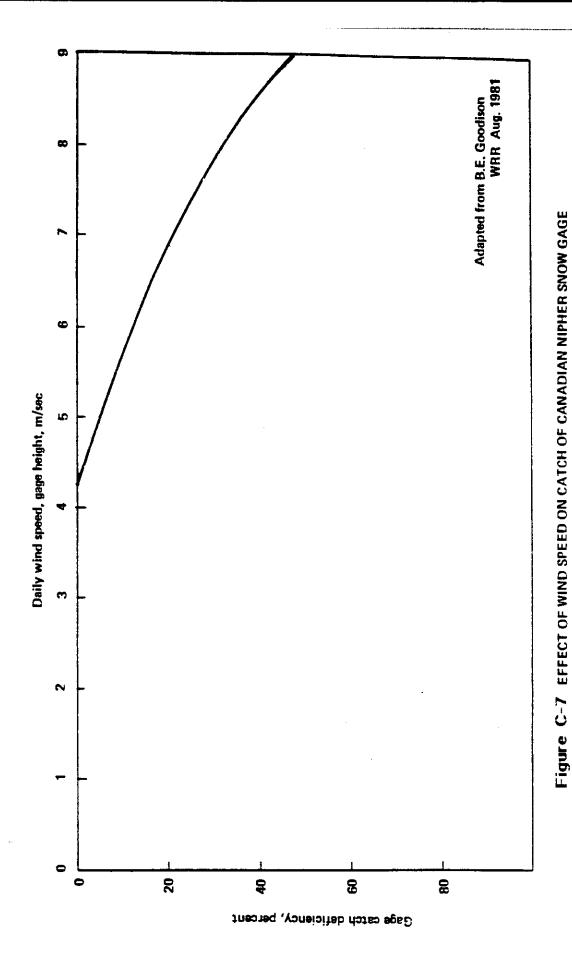


Figure C-4 FOR COMPUTATION OF DEFICIENCY IN CATCH OF RAIN, U.S. PRECIPITATION GAGES







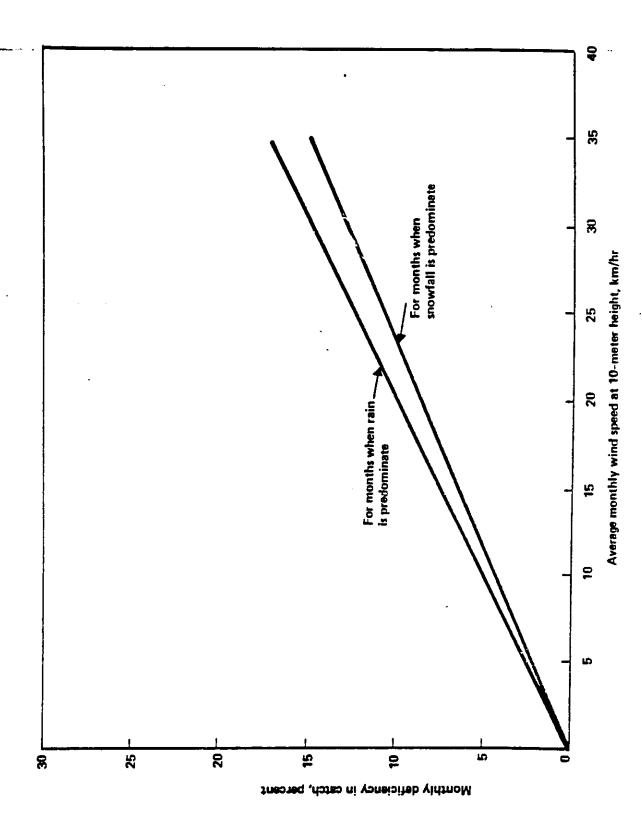


Figure C-8 FOR COMPUTATION OF DEFICIENCY IN MONTHLY CATCH OF RAIN, CANADIAN STANDARD RAIN GAGE.

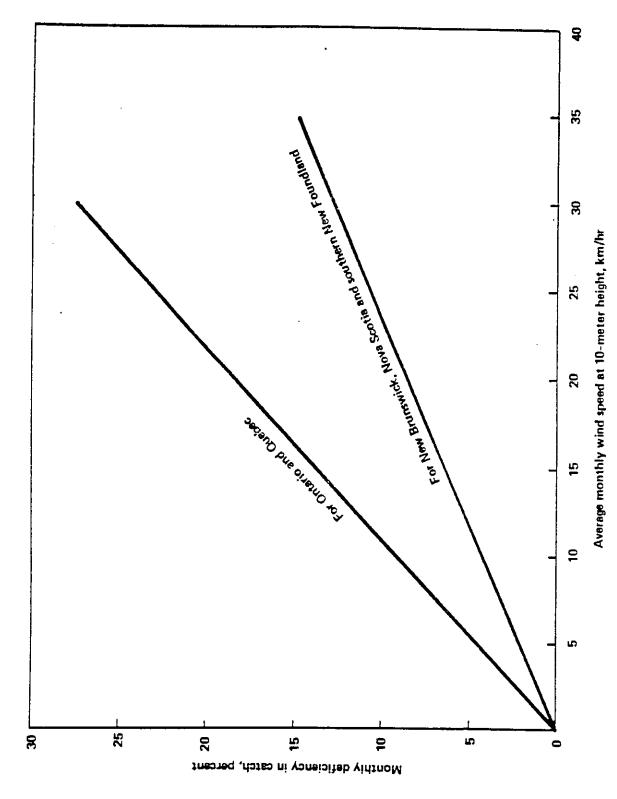


Figure C-9 FOR COMPUTATION OF DEFICIENCY IN MONTHLY CATCH OF SNOWFALL, CANADIAN NIPHER GAGE

## Hydrometeorological Data Collection Design and Analysis for the Lake Ontario Drainage Basin

## FINAL REPORT - PHASE I MAY 24, 1991

ATTACHMENT D

#### CONSISTENCY AND QUALITY EVALUATION OF RECORDS

### QUALITY OF GROUND SNOW SURVEY RECORDS

One of the primary objectives of this study is to check all records for consistency and to evaluate the quality of the records. As discussed in the main report, quality evaluation of the ground snow surveys records will be accomplished during Phase II and Phase III because of the limited number of airborne snow surveys now available.

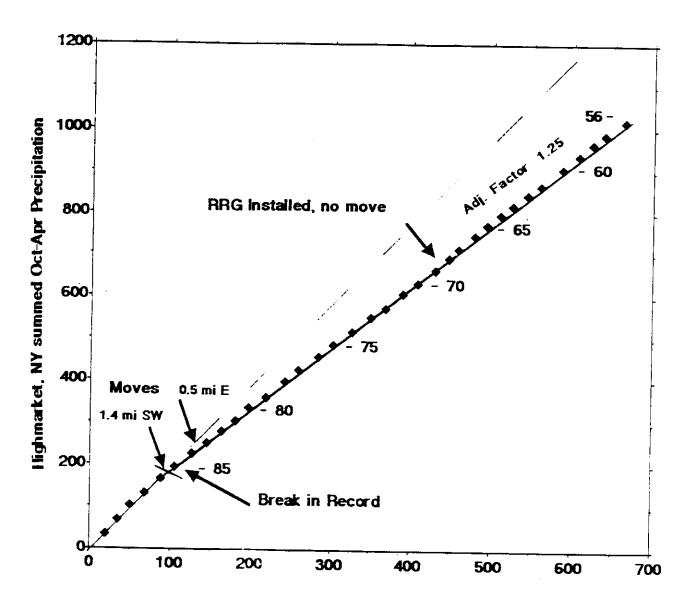
### **CONSISTENCY OF PRECIPITATION RECORDS**

The double mass analysis technique is being used for the first check on consistency of the precipitation and other hydrometeorological records. Many of the US and Canadian precipitation records have been analyzed. A primary reason for inconsistency in a record is a result of moves in the location of the gage or changes in the type of equipment. The inconsistency in the precipitation measurements may be due to differences in exposure of the precipitation gage as discussed in Attachment C,

Experience has shown that several months of the winter period are normally best suited to use as a base in the double mass analysis technique. For this reason, the winter period October - April has been selected for the initial analyses. These plots often shows inconsistencies in the records that correlates with the changes indicated in the station history files. Most of the errors in measurement of snow occurs when the precipitation is in the form of snow. In the US portion of the Lake Ontario drainage area this is primarily during the months of December through February.

Initial October-April double-mass analyses for the US precipitation stations have indicated that a large percentage of stations are inconsistent. Analyses to date show much less inconsistency in the Canadian precipitation records. Separate double-mass plots of December-February precipitation against base values (as well as comparison by the ratio method) are being prepared for stations showing inconsistencies.

An example of a double-mass analysis of October-April precipitation for the Highmarket, New York station is shown in Figure D-1. The adjustment factor found for the period Oct-Apr for 1956 through 1984 was 1.25. Part of the difference in relative catch for the two periods (at different locations) could be for other than under catch. It should also be noted that most of the under catch of snowfall would occur during the months of December through February so adjustment factors for these months would be greater than the 1.25 found for the October-April period.



Summed Oct-Apr Precipitation, Average of Base Stations

Figure D-1 Double Mass Plot of Highmarket, NY Oct-Apr Precipitation with Average of Base Stations

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